

## <u>\*PRELIMINARY\*</u> <u>SITE PLAN APPLICATION</u> City of Rochester, New Hampshire

| Check one of the following: 🖾 Design Review 📋 Conceptual (design review is strongly encouraged)                     |
|---|
| Property information  |
| Tax map #: 132; Lot #('s): 39; Zoning district: Residential   |
| Property address/location: 25 Old Dover Road ; # acres: 2.35  |
| Name of project (if applicable):  |
| Proposed project  |
| Describe proposed project: Subdivide the lot into two parcels. Parcel 1 to include the existing building & parking. |
| Parcel 2 for proposed 10,700 S.F. retail development.   |
| Nonresidential: current bldg. size 70,656 s.f.; total proposed bldg. size 10,700 s.f.                               |
| Residential: current # units total proposed # units   |
| City water? yes x no ; how far is City water from the site? Front of site   |
| City sewer? yes x no ; how far is City sewer from the site? Front of site   |
| Property owner  |
| Name (include name of individual): SWD Property Management LLC. Attn. Brian Dumont . Steve Dumont                   |
| Mailing address: PO Box 716, Exeter, NH 03833 - 73 PICKERING ROAD -54-17- 203                                       |
| Telephone #: 603 - 926 - 9029 Email: Steve & Dumont Prove Control Congup. 1 cm                                      |
| Applicant/developer (if different from property owner)  |
| Name (include name of individual): Dumont Properties, Attn. Brian Dumont / Steve Duwont                             |
| Mailing address: 73 Pickering Road, Suite 203, Rochester, NH 03839  |
| Telephone #: 603-661-2919 Email: bwdumontproperties@gmail.com   |
| Engineer/surveyor   |
| Name (include name of individual): Jones & Beach Engineers, Attn. Wayne Morrill                                     |
| Mailing address: PO Box 219, Stratham, NH 03885   |
| Telephone #: 603-772-4746 Fax #:  |
| Email address: wmorrill@jonesandbeach.com   |

Signature

24-24 Date\_\_\_\_

## Authorization to enter subject property

I hereby authorize members of the Rochester Planning Board, Zoning Board of Adjustment, Conservation Commission, Planning Department, and other pertinent City departments, boards and agencies to enter my property for the purpose of evaluating this application including performing any appropriate inspections during the application phase, review phase, post-approval phase, construction phase, and occupancy phase. This authorization applies specifically to those particular individuals legitimately involved in evaluating, reviewing, or inspecting this specific application/project. It is understood that these individuals must use all reasonable care, courtesy, and diligence when entering the property.

Signature of property owner:

Date: 1 - 24 - 24 at

### Letter of Authorization

I, Brian Dumont, Dumont Properties, 73 Pickering Road, Suite 203, Rochester, NH 03839, developer of property located in Rochester, NH, known as Tax Map 132, Lot 39, do hereby authorize Jones & Beach Engineers, Inc., PO Box 219, Stratham, NH, to act on my behalf concerning the previously mentioned property. The parcel is located at 25 Old Dover Road in Rochester, NH.

I hereby appoint Jones & Beach Engineers, Inc., as my agent to act on my behalf in the review process, to include any required signatures.

ion

Brian Dumont **Dumont Properties** 

n.

1-74-24 Date

JONES& BEACH

12

### Letter of Authorization

I, Brian Dumont, SWD Property Management LLC, PO Box 716, Exeter, NH 03833, owner of property located in Rochester, NH, known as Tax Map 132, Lot 39, do hereby authorize Jones & Beach Engineers, Inc., PO Box 219, Stratham, NH, to act on my behalf concerning the previously mentioned property. The parcel is located at 25 Old Dover Road in Rochester, NH.

I hereby appoint Jones & Beach Engineers, Inc., as my agent to act on my behalf in the review process, to include any required signatures.

Olow Mer, 1-24-24 Date A Onon **Brian Dumont** 

SWD Property Management LLC



## ABUTTERS LIST (DIRECT) AS OF JANUARY 2, 2024 FOR 25 OLD DOVER ROAD, ROCHESTER, NH JBE PROJECT No. 23050

#### **OWNER OF RECORD:**

TAX MAP 132/ LOT 39 SWD PROPERTY MANAGEMENT LLC ATTN. BRIAN DUMONT PO BOX 716 EXETER, NH 03833 BK 2885/PG 37 (10/22/03)

#### **APPLICANT:**

DUMONT PROPERTIES ATTN. BRIAN DUMONT 73 PICKERING RD, STE. 203 ROCHESTER, NH 03839

#### **ABUTTERS:**

131/1 & 2 HALEY & RICHARD PARTNERS 724 COLUMBUS AVE ROCHESTER, NH 03867 3043/379 (08/02/04)

131/3 KEVIN SIPULA 736 COLUMBUS AVE ROCHESTER, NH 03867 5019/499 (03/25/22)

132/26 KENNETH POULIN 20 OLD DOVER RD ROCHESTER, NH 03867 1873/270 (06/26/96) 132/37 RUTH WALLINGFORD 22 OLD DOVER RD ROCHESTER, NH 03867 842/293 (05/14/68)

### 132/28

MICHAEL ELDRIDGE 24 OLD DOVER RD ROCHESTER, NH 03867 4882/532 (03/17/21)

#### 132/29

MICHAEL & MARCIA MAHAN 14 BRIALLIA CIRCLE NEWMARKET, NH 03857 4839/673 (11/30/20)

### 132/30

DENNIS & CHERYL THOMPSON 28 OLD DOVER RD ROCHESTER, NH 03867 3232/906 (08/01/05)

### 132/31-23

STEVEN K MCENTIRE FAM TRUST % STEVEN K MCENTIRE TRUSTEE 115 MERRYMEETING RD NEW DURHAM, NH 03855 4841/820 (10/09/20)

### 132/36

CITY OF ROCHESTER 31 WAKEFIELD ST ROCHESTER, NH 03867 1379/483 (05/15/87)

#### 132/37 & 38 41 OLD DOVER ROAD LLC

41 OLD DOVER RD ROCHESTER, NH 03867 4007/189 (04/04/12) – LOT 37 4175/998 (10/15/13) – LOT 38 132/40 NORTHEAST CREDIT UNION % ACCOUNTING DEPT PO BOX 1240 PORTSMOUTH, NH 03802 2913/282 (12/10/03)

132/45 710 COLUMBUS AVENUE LLC 112 GATES ST PORTSMOUTH, NH 03801 4484/94 (06/10/17)

### **ENGINEERS/SURVEYORS:**

JONES & BEACH ENGINEERS, INC. ATTN: WAYNE MORRILL PO BOX 219 STRATHAM, NH 03885



## **City of Rochester, New Hampshire**

Zoning Board of Adjustment

August 14, 2023

SWD Property Management, LLC PO Box 716 Exeter, NH 03833

## Notice of Decision

Z-23-17 SWD Property Management, LLC Seeks a Variance from Table 18-B to permit the construction of a 10,700 s.f. retail building in the R2 zone where the use is not permitted.

Location: 25 Old Dover Road, Map 132 Lots 39 in the Residential-2 Zone.

At its August 9, 2023 meeting, the Zoning Board of Adjustment <u>APPROVED the Variance</u> as presented citing the criteria has been met, as described by the applicant.

NODA 8.14.23 Shanna B. Saunders,

Director of Planning Development

It is the applicant's responsibility to obtain any applicable permits from local, state, and federal agencies. Any work completed within the thirty (30) day appeal period, explained below, is at your risk.

**APPEALS**: Any party to the action, or any person directly affected has a right to appeal this decision within thirty calendar days following a hearing and to the Superior Court in accordance with State Statute. See New Hampshire Revised Statutes Annotated, Chapter 677 Rehearing and Appeal Procedures, available at the City of Rochester Planning Department This notice has been placed on file and made available for public inspection in the records of the ZBA.

Cc: Open Gov Z-23-15 File

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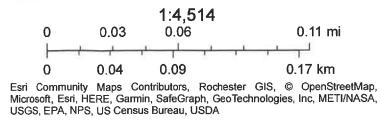


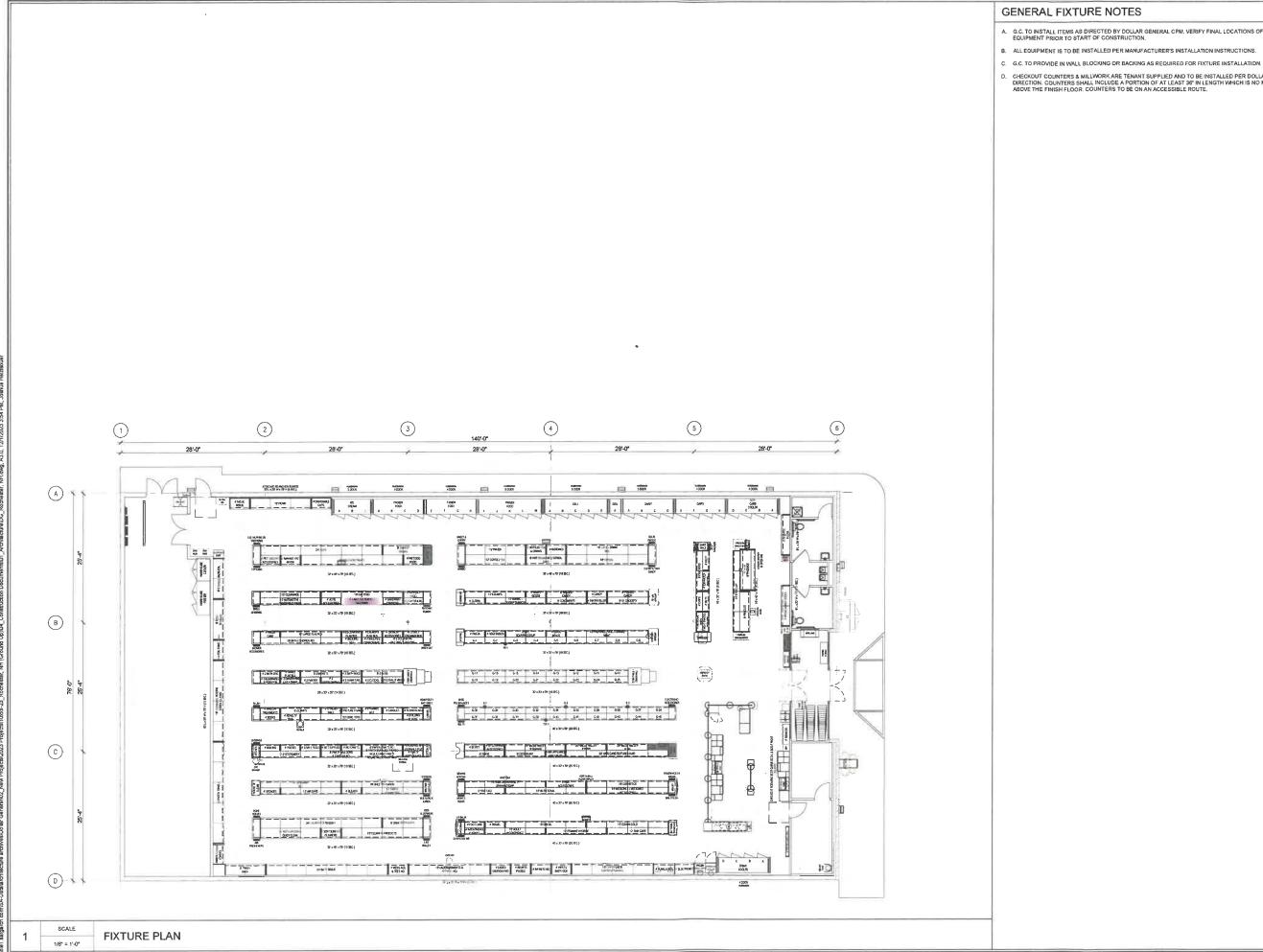
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Tax Parcels

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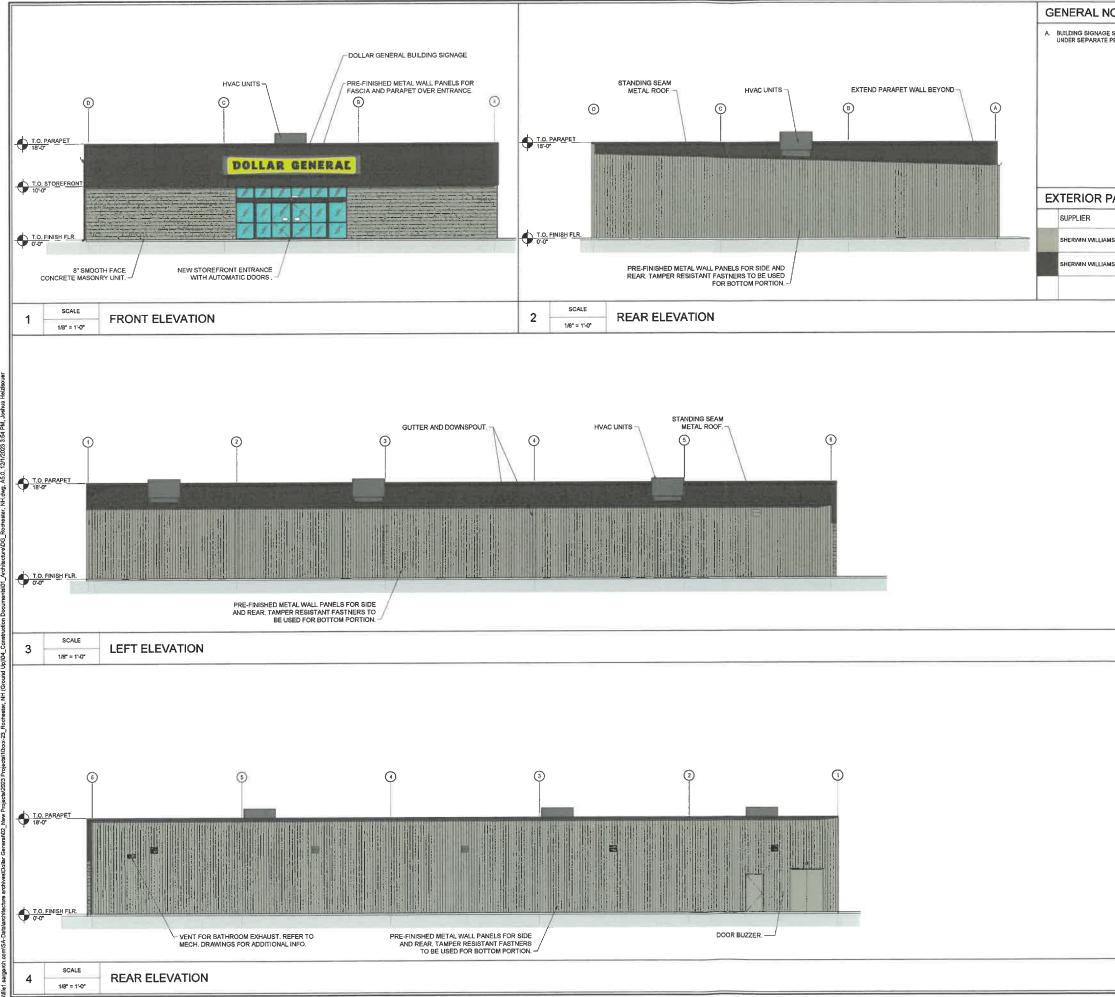
#### GENERAL FIXTURE NOTES

A. G.C. TO INSTALL ITEMS AS DIRECTED BY DOLLAR GENERAL CPM. VERIFY FINAL LOCATIONS OF FIXTURES AND EQUIPMENT PRIOR TO START OF CONSTRUCTION.

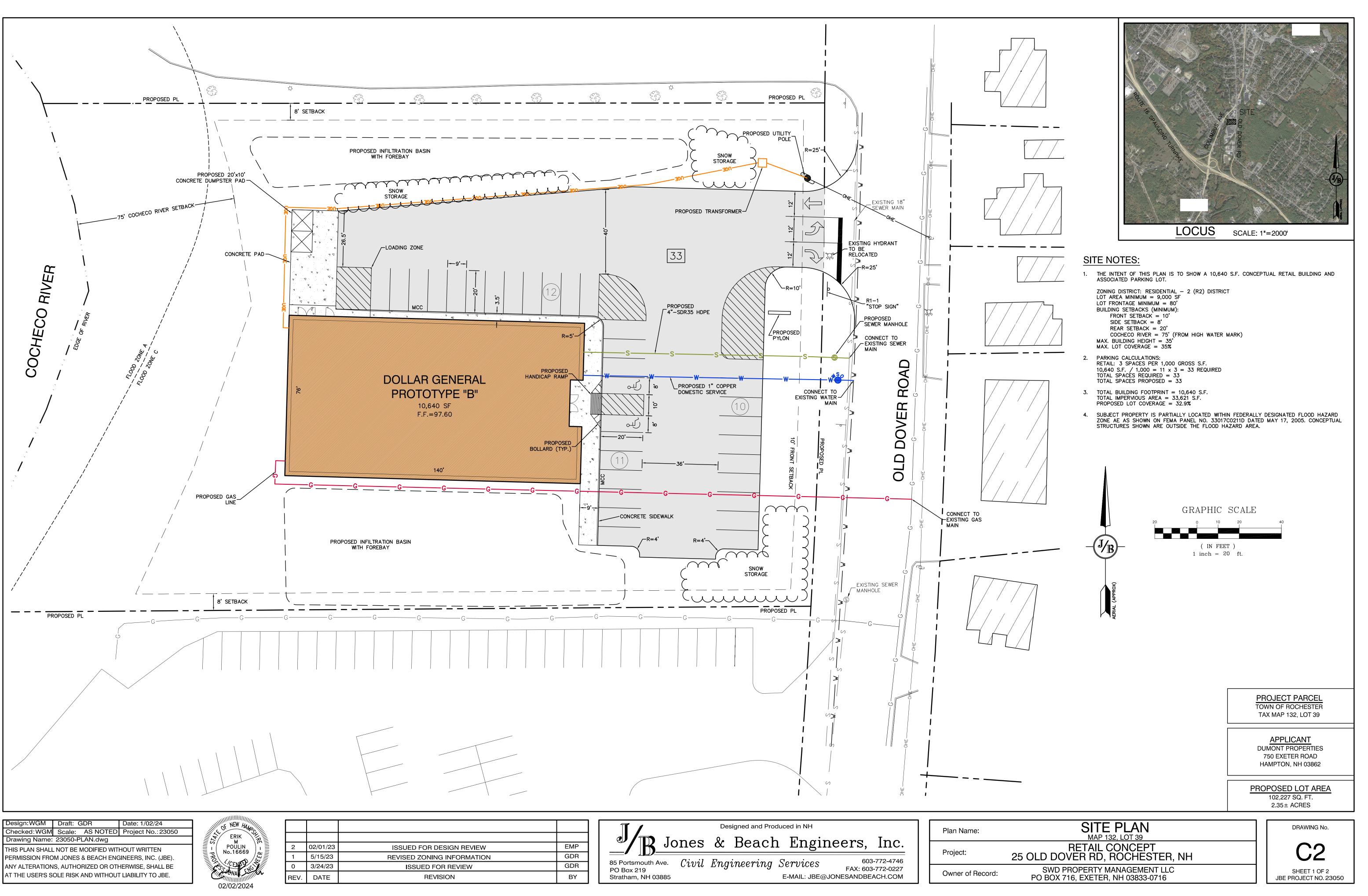
B. ALL EQUIPMENT IS TO BE INSTALLED PER MANUFACTURER'S INSTALLATION INSTRUCTIONS.

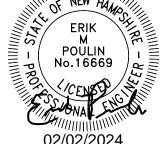
D. CHECKOUT COUNTERS & MILLWORK ARE TENANT SUPPLIED AND TO BE INSTALLED PER DOLLAR GENERAL CPM DIRECTION. COUNTERS SHALL INCLUDE A PORTION OF AT LEAST 36" IN LENGTH WHICH IS NO MORE THEN 34" ABOVE THE FINISH FLOOR. COUNTERS TO BE ON AN ACCESSIBLE ROUTE.



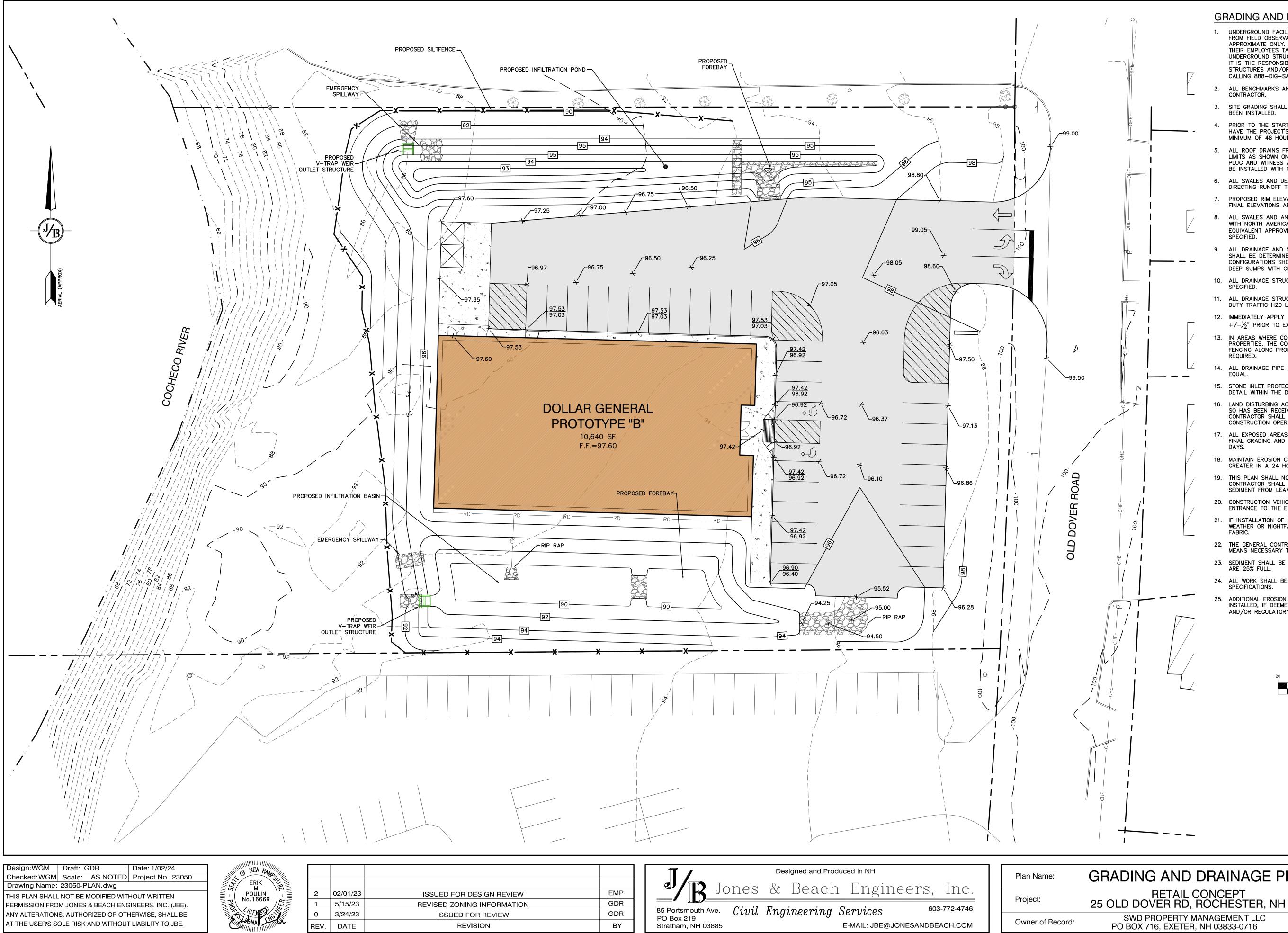


| DTES  |   |  |  |  |  |  |
|---|---|--|--|--|--|--|
| AINT SCHEDULE COLOR S #SW7037 BALANCED BEIGE S #SW7041 VAN DYKE BROWN | AREAS ALL*HIGH* PORTIONS OF BUILDING. COORDINATE WITH PM. | ASI FROM ROAD, PARAMUS, NJ 07652<br>TJ773.253.9393 • WWW.LARGAREN.COM<br>ARCHITECTURAL SEAL:<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.5111<br>NO.511 |  |  |  |  |
|   |   | CONTRACTOR'S NOTES:<br>WRITTEN DIMENSIONS HOLD<br>PREFERENCE OVER SCALE DI<br>DIMENSIONS: DO NOT SCALE THE<br>DIMENSIONS: THE CONTRACTORS INVESTIGATIONS<br>SCHEMITTING BLOSS. REPORT: ANY<br>DISCREMENTING BLOSS.<br>DISCREMENTING BLOSS. REPORT: ANY<br>DISCREMENTING BLOSS.<br>DISCREMENTING BLOSS. REPORT: ANY<br>DISCREMENTING BLOSS.<br>DISCREMENTING BLOSS.<br>DISCREMENTI  |  |  |  |  |
|   |   | SHEET NUMBER:  |  |  |  |  |





| 2    | 02/01/23 | ISSUED FOR DESIGN REVIEW  |
|------|----------|---------------------------|
| 1    | 5/15/23  | REVISED ZONING INFORMATIC |
| 0    | 3/24/23  | ISSUED FOR REVIEW         |
| REV. | DATE     | REVISION                  |
|      |          |                           |





| 2    | 02/01/23 | ISSUED FOR DESIGN REVIEV  |
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| 1    | 5/15/23  | REVISED ZONING INFORMATIC |
| 0    | 3/24/23  | ISSUED FOR REVIEW         |
| REV. | DATE     | REVISION                  |

## **GRADING AND DRAINAGE NOTES:**

- UNDERGROUND FACILITIES, UTILITIES AND STRUCTURES HAVE BEEN PLOTTED FROM FIELD OBSERVATION AND THEIR LOCATION MUST BE CONSIDERED APPROXIMATE ONLY. NEITHER JONES & BEACH ENGINEERS, INC., NOR ANY OF THEIR EMPLOYEES TAKE RESPONSIBILITY FOR THE LOCATION OF ANY UNDERGROUND STRUCTURES AND/OR UTILITIES NOT SHOWN THAT MAY EXIST. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO HAVE ALL UNDERGROUND STRUCTURES AND/OR UTILITIES LOCATED PRIOR TO EXCAVATION WORK BY CALLING 888-DIG-SAFE (888-344-7233).
- ALL BENCHMARKS AND TOPOGRAPHY SHOULD BE FIELD VERIFIED BY THE 2. CONTRACTOR.
- 3. SITE GRADING SHALL NOT PROCEED UNTIL EROSION CONTROL MEASURES HAVE BEEN INSTALLED.
- 4. PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR IS REQUIRED TO HAVE THE PROJECT'S LAND SURVEYOR STAKE OR FLAG CLEARING LIMITS. A MINIMUM OF 48 HOURS NOTICE IS REQUIRED.
- 5. ALL ROOF DRAINS FROM BUILDING SHALL END 5' OUTSIDE THE BUILDING LIMITS AS SHOWN ON PLAN AND SHALL BE PROVIDED WITH A TEMPORARY PLUG AND WITNESS AT THE END. ALL EXTERIOR ROOF DOWNSPOUTS ARE TO BE INSTALLED WITH OVERFLOW DEVICES.
- 6. ALL SWALES AND DETENTION PONDS ARE TO BE STABILIZED PRIOR TO DIRECTING RUNOFF TO THEM.
- PROPOSED RIM ELEVATIONS OF DRAINAGE STRUCTURES ARE APPROXIMATE. 7. FINAL ELEVATIONS ARE TO BE SET FLUSH WITH FINISH GRADES.
- ALL SWALES AND ANY SLOPES GREATER THAN 3:1 SHALL BE STABILIZED 8. WITH NORTH AMERICAN GREEN S75 EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER), UNLESS OTHERWISE SPECIFIED.
- ALL DRAINAGE AND SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN) 9. SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS SHOWN ON THESE PLANS. CATCH BASINS SHALL HAVE 3' DEEP SUMPS WITH GREASE HOODS, UNLESS OTHERWISE NOTED.
- 10. ALL DRAINAGE STRUCTURES SHALL BE PRECAST, UNLESS OTHERWISE SPECIFIED.
- 11. ALL DRAINAGE STRUCTURES AND STORM SEWER PIPES SHALL MEET HEAVY DUTY TRAFFIC H20 LOADING AND SHALL BE INSTALLED ACCORDINGLY.
- 12. IMMEDIATELY APPLY AND COMPACT STONE BASE FOR BUILDING PAD TO  $+/-\frac{1}{2}$ " PRIOR TO EXCAVATING INTERIOR AND PERIMETER FOOTINGS.
- 13. IN AREAS WHERE CONSTRUCTION IS PROPOSED ADJACENT TO ABUTTING PROPERTIES, THE CONTRACTOR SHALL INSTALL ORANGE CONSTRUCTION FENCING ALONG PROPERTY LINES IN ALL AREAS WHERE SILT FENCING IS NOT REQUIRED.
- 14. ALL DRAINAGE PIPE SHALL BE NON-PERFORATED ADS N-12 OR APPROVED EQUAL.
- 15. STONE INLET PROTECTION SHALL BE PLACED AT ALL CATCH BASINS. SEE DETAIL WITHIN THE DETAIL SHEETS.
- 16. LAND DISTURBING ACTIVITIES SHALL NOT COMMENCE UNTIL APPROVAL TO DO SO HAS BEEN RECEIVED BY ALL GOVERNING AUTHORITIES. THE GENERAL CONTRACTOR SHALL STRICTLY ADHERE TO THE EPA SWPPP DURING CONSTRUCTION OPERATIONS.
- 17. ALL EXPOSED AREAS SHALL BE SEEDED AS SPECIFIED WITHIN 3 DAYS OF FINAL GRADING AND ANYTIME CONSTRUCTION STOPS FOR LONGER THAN 3 DAYS.
- 18. MAINTAIN EROSION CONTROL MEASURES AFTER EACH RAIN EVENT OF 0.5" OR GREATER IN A 24 HOUR PERIOD AND AT LEAST ONCE A WEEK.
- 19. THIS PLAN SHALL NOT BE CONSIDERED ALL INCLUSIVE, AS THE GENERAL CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PREVENT SEDIMENT FROM LEAVING THE SITE.
- 20. CONSTRUCTION VEHICLES SHALL UTILIZE THE STABILIZED CONSTRUCTION ENTRANCE TO THE EXTENT POSSIBLE THROUGHOUT CONSTRUCTION.
- 21. IF INSTALLATION OF STORM DRAINAGE SYSTEM SHOULD BE INTERRUPTED BY WEATHER OR NIGHTFALL, THE PIPE ENDS SHALL BE COVERED WITH FILTER FABRIC.
- 22. THE GENERAL CONTRACTOR SHALL BE RESPONSIBLE TO TAKE WHATEVER MEANS NECESSARY TO ESTABLISH PERMANENT SOIL STABILIZATION.
- 23. SEDIMENT SHALL BE REMOVED FROM ALL SEDIMENT BASINS BEFORE THEY ARE 25% FULL.
- 24. ALL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH PROJECT SPECIFICATIONS.
- 25. ADDITIONAL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE INSTALLED, IF DEEMED NECESSARY BY ON-SITE INSPECTION BY ENGINEER AND/OR REGULATORY OFFICIALS.

GRAPHIC SCALE ( IN FEET )

1 inch = 20 ft.

PROJECT PARCEL TOWN OF ROCHESTER TAX MAP 132, LOT 39

APPLICANT DUMONT PROPERTIES 750 EXETER ROAD HAMPTON, NH 03862

**PROPOSED LOT AREA** 102,227 SQ. FT.  $2.35 \pm ACRES$ 

# **GRADING AND DRAINAGE PLAN**

SWD PROPERTY MANAGEMENT LLC

PO BOX 716, EXETER, NH 03833-0716

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SHEET 2 OF 2

JBE PROJECT NO. 23050

DRAWING No.

## **TRAFFIC IMPACT STATEMENT**

## **ITE TRIP GENERATION MEMORANDUM**

Retail Development Tax Map 132, Lot 39 25 Old Dover Road Rochester, NH

**Prepared for:** 

Dumont Properties 750 Exeter Road Hampton, NH 03862

> Prepared by: Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 August 8, 2023 Revised January 4, 2024 JBE Project No. 23050

## **EXECUTIVE SUMMARY**

The intent of this project is to construction a 10,700 S.F. retail store with associated parking areas. The intent of this report is to evaluate the potential impacts on adjacent street traffic that this development would have on an average day.

Data from the Institute of Transportation Engineers (ITE) Trip Generation Manual, 10<sup>th</sup> Edition (ITE Manual) were used. The Land Use in the ITE Manual that most nearly matches the retail use is "Variety Store" (Land Use 814), defined by the ITE Manual as follows: "A variety store is a retail store that sells a broad range of inexpensive items often at a single price. These stores are typically referred to as 'dollar stores'". A dollar store is proposed for the property, so this land use code is a fitting one.

The estimates for the retail use were calculated from data from the ITE Manual based on the average number of trips generated per 1,000 S.F. gross floor area. Sometimes the ITE Manual is able to provide weekday as well as weekend trip generation estimates. However, for Land Use 814 only weekday trip generation estimates were available. The available estimates were for a full day, as well as the estimates for the peak hour of the generating use and the peak hour of adjacent street traffic.

Because a 10,700 SF retail use is proposed, the number of trips per 1,000 SF GFA was multiplied by 10.7 to come up with the estimated trip generation. The below table summarizes the average estimated traffic associated with the proposed use according to traffic from the ITE Manual:

| Tretage Trip Generation Estimates |                      |                            |                           |  |  |  |  |
|-----------------------------------|----------------------|----------------------------|---------------------------|--|--|--|--|
|                                   | Full Day (Trips/Day) | <b>Peak Hour Generator</b> | <b>Peak Hour Adjacent</b> |  |  |  |  |
|                                   |                      | (Trips/Hour)               | Street (Trips/Hour)       |  |  |  |  |
| Weekday                           | 679                  | N/A                        | N/A                       |  |  |  |  |
| Weekday AM                        | N/A                  | 48.4                       | 34.0                      |  |  |  |  |
| Weekday PM                        | N/A.                 | 80.0                       | 73.2                      |  |  |  |  |

**Average Trip Generation Estimates** 

## CONCLUSION

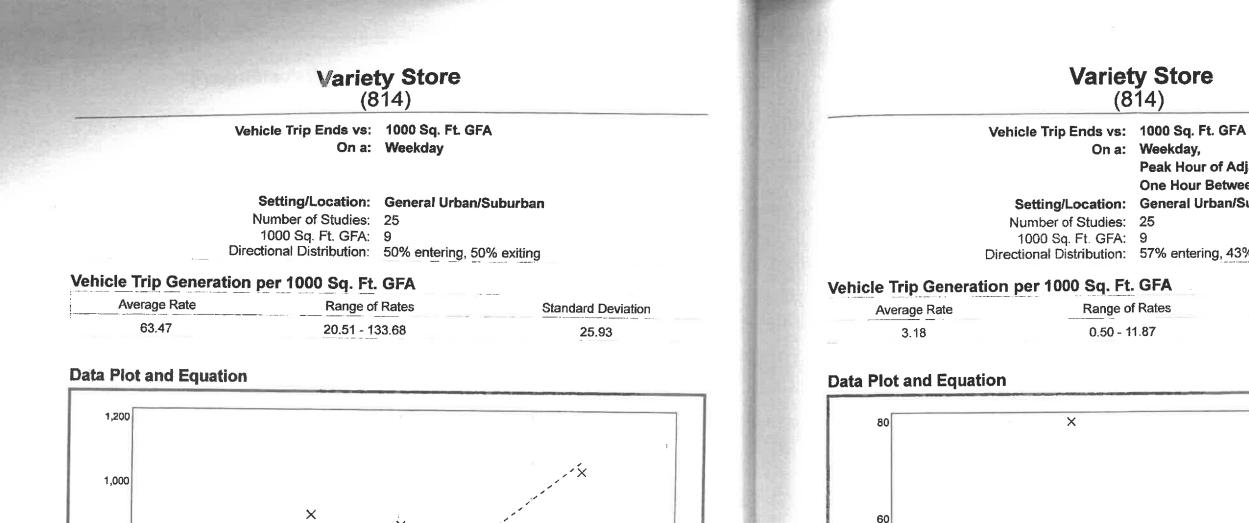
Assuming 12 hours of operation per day, there would be an average of one trip entering or leaving the site every 64 seconds (one trip every minute, essentially). During the weekday PM peak hour of the generating use, which is the highest peak hour scenario available, 80 trips through the hour translates to one trip entering or leaving every 45 seconds based on ITE estimates for average trip generation. Because these are averages, on a particularly busy day there may be more traffic entering or leaving, and on a less busy day there would be fewer than the reported number of trips. Regardless, it appears that there will be appreciable time between entrances into and exits from the site. It is not anticipated that this will cause a significant impact on the traffic of Old Dover Road, which already experiences a moderate amount of traffic due to its proximity to several existing businesses.

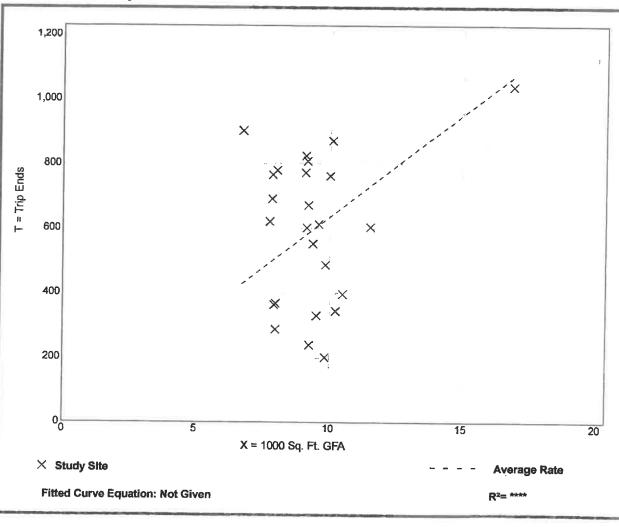
Respectfully submitted, **JONES & BEACH ENGINEERS, INC.** 

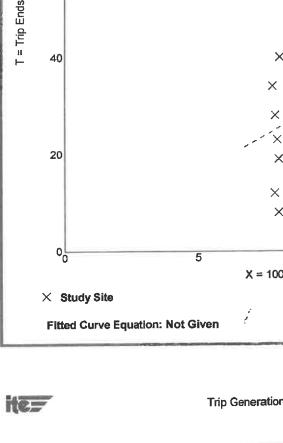
Wayne Morrill

President

Trip generation estimates used for this analysis were taken from the Trip Generation Manual, 10<sup>th</sup> Edition, published by the Institute of Traffic Engineers in September 2017.







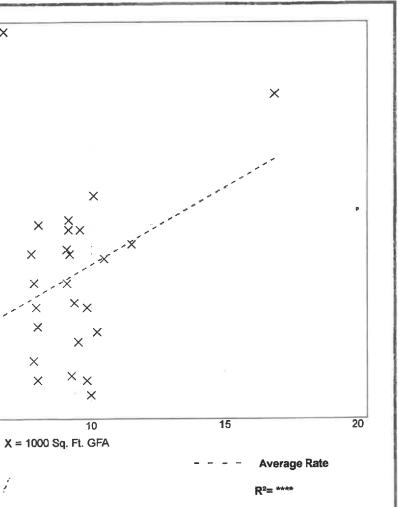
38 Trip Generation Manual 10th Edition • Volume 2: Data • Retail (Land Uses 800-899)

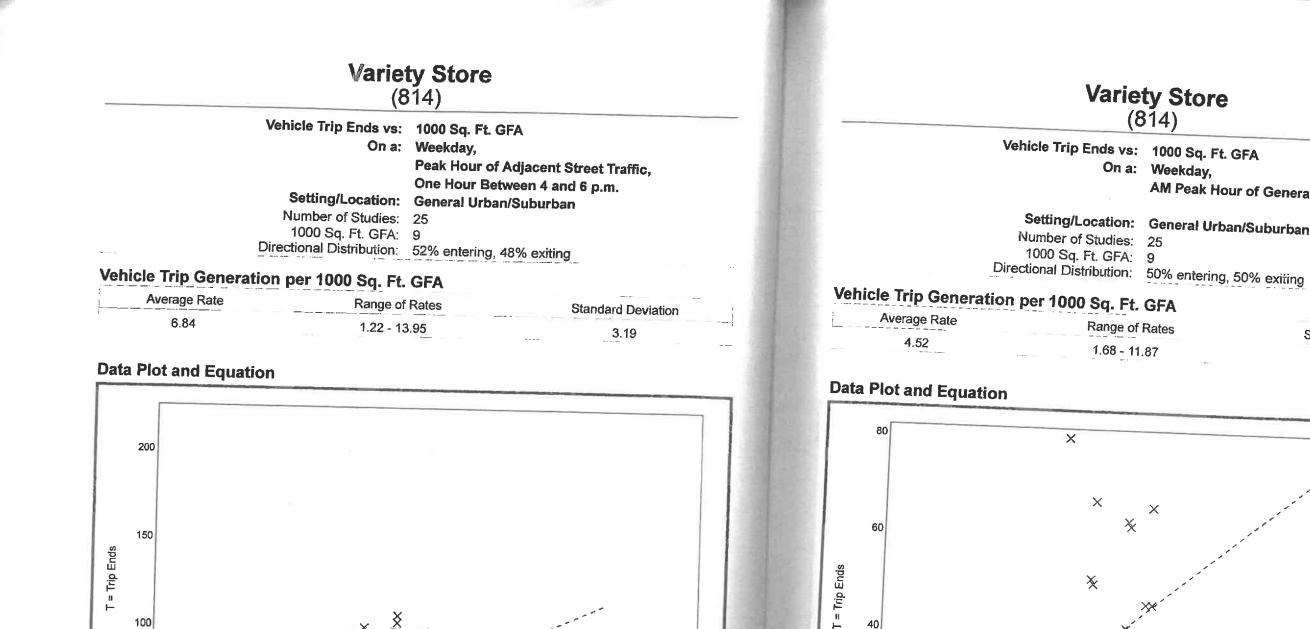
# Variety Store (814)

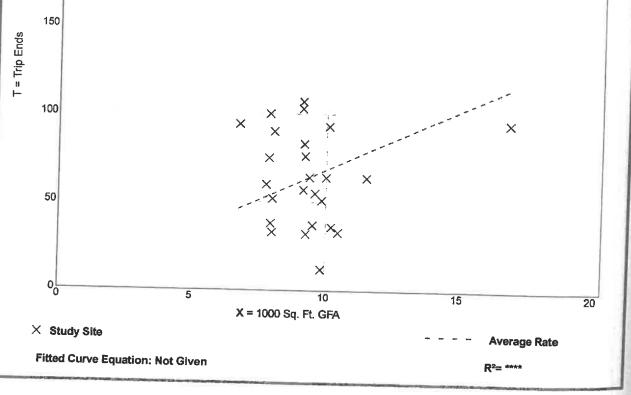
On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. Setting/Location: General Urban/Suburban

- Directional Distribution: 57% entering, 43% exiting

| nge of Rates | Standard Deviation | į |
|--------------|--------------------|---|
| 50 - 11.87   | 2.01               |   |







Trip Generation Manual 10th Edition • Volume 2: Data • Retail (Land Uses 800-899)

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imes Study Site

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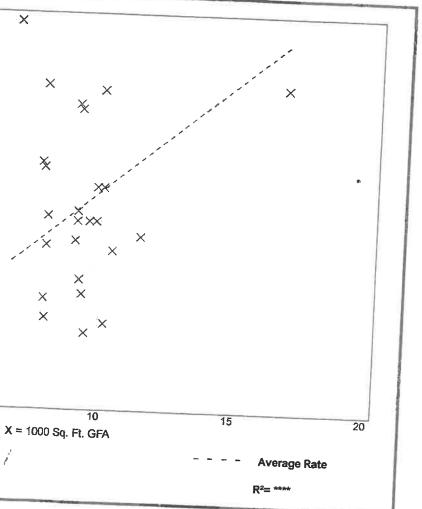
Fitted Curve Equation: Not Given

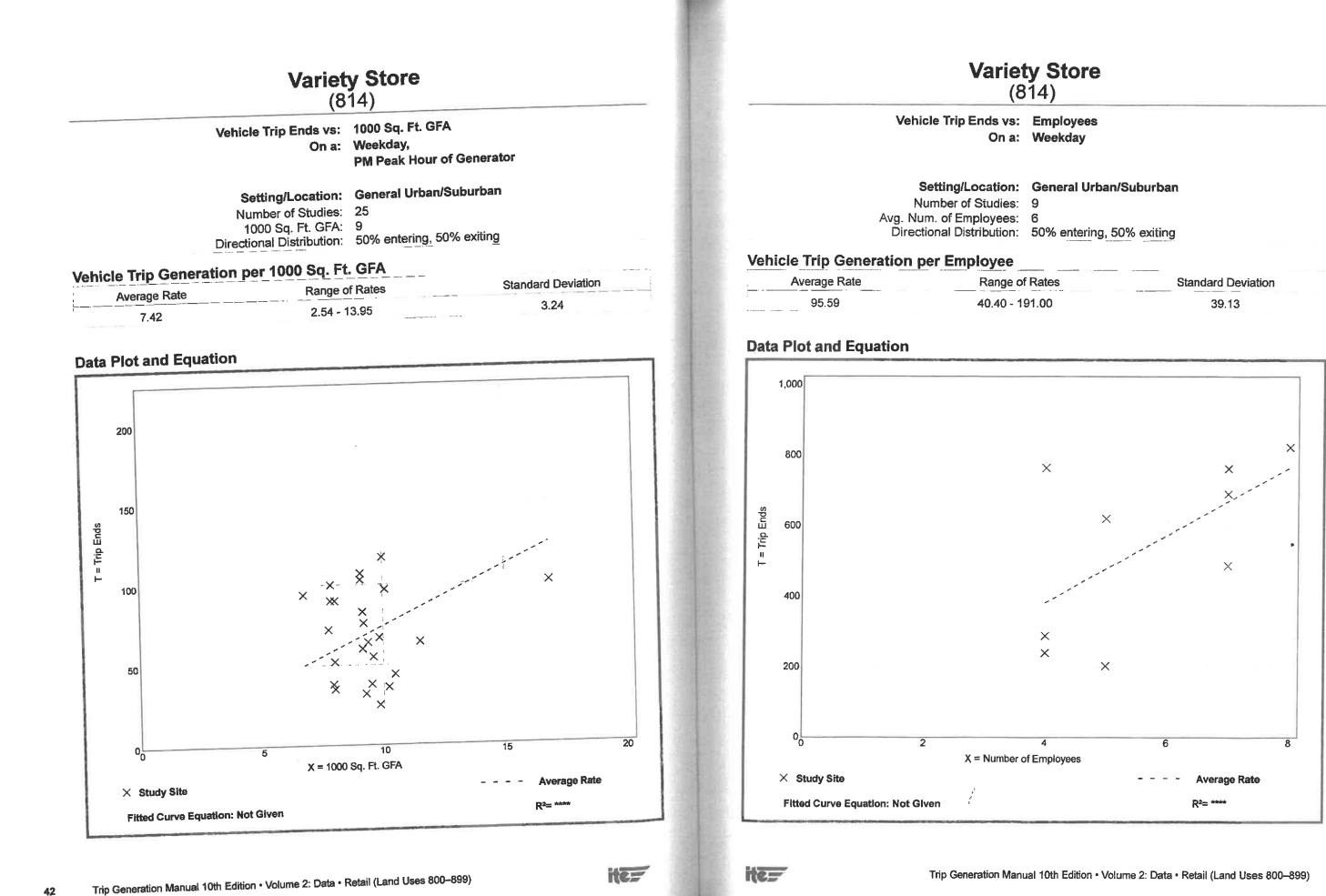
## Variety Store (814)

On a: Weekday, AM Peak Hour of Generator

- Setting/Location: General Urban/Suburban

Range of Rates Standard Deviation 1.68 - 11.87 2.13





| :  | General Urban/Suburba    | in              |
|----|--------------------------|-----------------|
| :  | 9                        |                 |
| :  | 6                        |                 |
| :  | 50% entering, 50% exitin | g               |
|    |                          |                 |
| of | Dates                    | Standard Doviat |

## **DRAINAGE ANALYSIS**

## SEDIMENT AND EROSION CONTROL PLAN

Dollar General Tax Map 132 Lot 39 25 Old Dover Road Rochester, NH

**Prepared for:** 

SWD Property Management LLC PO Box 716 Exeter, NH 03833



Prepared by: Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 February 01, 2023 JBE Project No. 23050

## **EXECUTIVE SUMMARY**

SWD Property Management LLC proposes to construct a  $10,640 \pm$  sq.ft. retail building on Old Dover Road, Rochester, NH. The existing lot, Tax Map 132 Lot 39, contains 2.35 acres. A drainage analysis of the site and its offsite contributing watershed areas was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (pre-development) condition, and a second for its proposed (post-development) condition. The analysis was conducted using data for the 2 Year – 24 Hour (3.08"), 10 Year – 24 Hour (4.63"), 25 Year – 24 Hour (5.84"), and 50 Year – 24 Hour (6.96") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. A summary of the existing and proposed conditions peak rates of runoff is as follows:

| COMPONENT         |        | PEAK RATE OF RUNOFF (CUBIC FEET/SECOND) |         |      |         |      |         |      |
|-------------------|--------|---|---------|------|---------|------|---------|------|
|                   | 2 Year |   | 10 Year |      | 25 Year |      | 50 Year |      |
|                   | Pre    | Post                                    | Pre     | Post | Pre     | Post | Pre     | Post |
| Analysis Point #1 | 0.00   | 0.00                                    | 0.12    | 0.04 | 0.56    | 0.42 | 1.35    | 0.94 |

The drainage design intent for this site is to maintain the post-development peak flow to the predevelopment peak flow conditions. This has been accomplished through the use of two infiltration ponds to mitigate the peak flow exiting the site.

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Executive Summary

- 1. Executive Summary
- 2. Stormwater Checklist
- 3. Drainage Analysis
  - 3.1. Introduction
  - 3.2. Methodology
  - 3.3. Existing Conditions Analysis
  - 3.4. Proposed Conditions Analysis
  - 3.5. Conclusion
- 4. Appendices

Appendix I – Existing Conditions Analysis

2 Year – 24 Hour Summary Analysis 10 Year – 24 Hour Complete Analysis 25 Year – 24 Hour Summary Analysis 50 Year – 24 Hour Summary Analysis

Appendix II – Proposed Conditions Analysis

2 Year – 24 Hour Summary Analysis 10 Year – 24 Hour Complete Analysis 25 Year - 24 Hour Summary Analysis 50 Year – 24 Hour Summary Analysis

| Web Soil Survey Map            |
|--------------------------------|
| Aerial Photograph of Site      |
| Drainage Plans                 |
| Pre-Development Drainage Plan  |
| Post-Development Drainage Plan |
|                                |

Proposed Retail Old Dover Road Drainage Analysis and Erosion and Sediment Control Plan Page 1

## **1.0 INTRODUCTION**

SWD Property Management LLC proposes to construct a  $10,640\pm$  sq.ft. retail building on Old Dover Road, Rochester, NH. The proposed site will be located on the west side of Old Dover Road. Site improvements include the construction of the proposed  $10,640\pm$  sq.ft retail building, construction of utilities, parking, and drainage improvements.

## 2.0 METHODOLOGY

The existing and proposed watersheds were modeled utilizing HydroCad stormwater software, version 9.10. The watersheds were analyzed utilizing the SCS TR-20 methodology for hydrograph development and the TR-55 methodology for Time of Concentration (Tc) determination. The Dynamic-Storage-Indicating method for reach and pond routing was utilized. Type III, 24-hour hydrographs were developed for the 2-year, 10-year, 25-year, and 50-year storm events corresponding to 3.08", 4.63", 5.84", and 6.96" rainfall storm events respectively as directed by the SCS *Technical Paper 40* (TP-40) and the *New Hampshire Stormwater Manual – Volume 2, Appendix A*.

Existing topography and site features were obtained through on-ground topography completed by Jones & Beach Engineers. Existing soil conditions were derived the Natural Resources Conservation Services (NRCS) Web Soil Service Mapping Tool.

## 3.0 EXISTING CONDITIONS ANALYSIS

The study area consists of the subject property and upstream contributing area. The contributing area contains 2.183 acres on the west side of Old Dover Road. The existing site consists of lightly wooded areas and grass areas.

The existing topography is such that the existing site drainage is one large watersheds that drains in in a Westerly path towards the Cocheco River.

Existing soil conditions were obtained from the NRCS Soils Maps. The existing soils are classified by the NRCS as Windsor Loamy Sand. These soils are classified as Hydrologic Group 'A'.

Given all discharge point converge quickly into one River system, one Analysis Point (AP) has been defined for this project. The watershed in AP-1 collects drainage from the entire project site, and discharges into the Cocheco River.

## 4.0 PROPOSED CONDITIONS ANALYSIS

SWD Property Management LLC proposes to construct a  $10,640 \pm$  sq.ft. retail building with associated municipal sewer and water and on-site parking.

The proposed site has been designed to sheet flow runoff to the proposed drainage system comprised of surface drainage directed to proposed infiltration basins.

Runoff from the entire site sheet flows west towards the proposed infiltration basins via surface sheet flow. This flow first enters forebays for pretreatment. The flow then discharges to the rear of the property towards the Cocheco River (AP #1).

As the table in the Executive Summary demonstrates, the proposed peak rates of runoff have been maintained at the existing peak rates of runoff for the analyzed storms to the extent practicable.

Treatment is obtained through the use of a sediment forebay, and infiltration basin. Sizing for forebay and infiltration basin are based upon NHDES requirements as described in Volume 2 of the Stormwater Handbook.

## 5.0 CONCLUSION

This proposed site development will have minimal adverse effect on abutting infrastructures or properties by way of stormwater runoff or siltation. Peak runoff rate from the proposed site has been maintained to the existing conditions peak rate to the extent practicable.

Respectfully Submitted, JONES & BEACH ENGINEERS, INC.

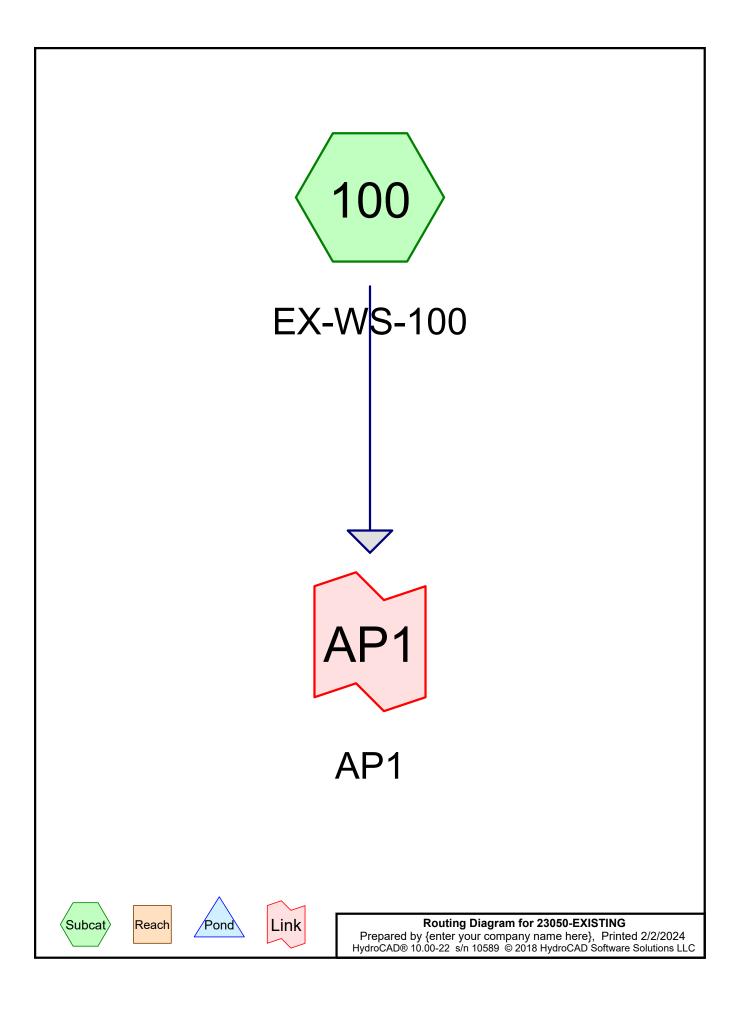
E-P-

Erik Poulin, P.E. Project Engineer

## APPENDIX I

## EXISTING CONDITIONS DRAINAGE ANALYSIS

2 YEAR Summary Analysis 10 YEAR Complete Analysis 25 YEAR Summary Analysis 50 YEAR Summary Analysis



## Area Listing (all nodes)

| Area    | CN | Description                   |
|---------|----|-------------------------------|
| (acres) |    | (subcatchment-numbers)        |
| 1.208   | 39 | GRASS COVER >75%, HSG A (100) |
| 0.078   | 96 | GRAVEL, HSG A (100)           |
| 0.067   | 98 | IMPERVIOUS, HSG A (100)       |
| 0.830   | 36 | WOODS, HSG A (100)            |
| 2.182   | 42 | TOTAL AREA                    |

## 23050-EXISTING

## Soil Listing (all nodes)

| Area    | Soil  | Subcatchment |
|---------|-------|--------------|
| (acres) | Group | Numbers      |
| 2.182   | HSG A | 100          |
| 0.000   | HSG B |              |
| 0.000   | HSG C |              |
| 0.000   | HSG D |              |
| 0.000   | Other |              |
| 2.182   |       | TOTAL AREA   |
| 0.000   | HSG D | TOTAL AREA   |

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

> Runoff Area=95,064 sf 3.05% Impervious Runoff Depth>0.01" Flow Length=358' Tc=10.0 min CN=42 Runoff=0.00 cfs 0.001 af

Link AP1: AP1

Subcatchment100: EX-WS-100

Inflow=0.00 cfs 0.001 af Primary=0.00 cfs 0.001 af

Total Runoff Area = 2.182 ac Runoff Volume = 0.001 af Average Runoff Depth = 0.01" 96.95% Pervious = 2.116 ac 3.05% Impervious = 0.067 ac Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

> Runoff Area=95,064 sf 3.05% Impervious Runoff Depth>0.22" Flow Length=358' Tc=10.0 min CN=42 Runoff=0.12 cfs 0.040 af

Link AP1: AP1

Subcatchment100: EX-WS-100

Inflow=0.12 cfs 0.040 af Primary=0.12 cfs 0.040 af

Total Runoff Area = 2.182 ac Runoff Volume = 0.040 af Average Runoff Depth = 0.22" 96.95% Pervious = 2.116 ac 3.05% Impervious = 0.067 ac

## Summary for Subcatchment 100: EX-WS-100

Runoff = 0.12 cfs @ 12.50 hrs, Volume= 0.040 af, Depth> 0.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.63"

|   | A     | rea (sf) | CN      | Description             |              |                                 |  |  |
|---|-------|----------|---------|-------------------------|--------------|---------------------------------|--|--|
| * |       | 52,614   | 39      | GRASS COVER >75%, HSG A |              |                                 |  |  |
| * |       | 36,150   | 36      | WOODS, H                | SG A         |                                 |  |  |
| * |       | 2,898    | 98      | IMPERVIO                | JS, HSG A    |                                 |  |  |
| * |       | 3,402    | 96      | GRAVEL, F               | ISG A        |                                 |  |  |
| _ |       | 95,064   | 42      | Weighted A              | verage       |                                 |  |  |
|   |       | 92,166   |         | 96.95% Pei              |              |                                 |  |  |
|   |       | 2,898    | ;       | 3.05% Impe              | ervious Area | а                               |  |  |
|   |       | ,        |         | •                       |              |                                 |  |  |
|   | Tc    | Length   | Slope   | Velocity                | Capacity     | Description                     |  |  |
|   | (min) | (feet)   | (ft/ft) | (ft/sec)                | (cfs)        |                                 |  |  |
|   | 6.7   | 100      | 0.0550  | 0.25                    |              | Sheet Flow,                     |  |  |
|   |       |          |         |                         |              | Grass: Short n= 0.150 P2= 3.08" |  |  |
|   | 0.8   | 68       | 0.0368  | 1.34                    |              | Shallow Concentrated Flow,      |  |  |
|   |       |          |         |                         |              | Short Grass Pasture Kv= 7.0 fps |  |  |
|   | 2.0   | 113      | 0.0177  | 0.93                    |              | Shallow Concentrated Flow,      |  |  |
|   |       |          |         |                         |              | Short Grass Pasture Kv= 7.0 fps |  |  |
|   | 0.5   | 77       | 0.2860  | 2.67                    |              | Shallow Concentrated Flow,      |  |  |
|   |       |          |         |                         |              | Woodland Kv= 5.0 fps            |  |  |
|   | 10.0  | 358      | Total   |                         |              |                                 |  |  |

## Summary for Link AP1: AP1

| Inflow Area | a = | 2.182 ac,  | 3.05% Impervious, | Inflow Depth > 0.2 | 22" for 10 YEAR event   |
|-------------|-----|------------|-------------------|--------------------|-------------------------|
| Inflow      | =   | 0.12 cfs @ | 12.50 hrs, Volume | = 0.040 af         |                         |
| Primary     | =   | 0.12 cfs @ | 12.50 hrs, Volume | = 0.040 af,        | Atten= 0%, Lag= 0.0 min |

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

> Runoff Area=95,064 sf 3.05% Impervious Runoff Depth>0.56" Flow Length=358' Tc=10.0 min CN=42 Runoff=0.56 cfs 0.102 af

Link AP1: AP1

Subcatchment100: EX-WS-100

Inflow=0.56 cfs 0.102 af Primary=0.56 cfs 0.102 af

Total Runoff Area = 2.182 ac Runoff Volume = 0.102 af Average Runoff Depth = 0.56" 96.95% Pervious = 2.116 ac 3.05% Impervious = 0.067 ac Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

> Runoff Area=95,064 sf 3.05% Impervious Runoff Depth>0.98" Flow Length=358' Tc=10.0 min CN=42 Runoff=1.35 cfs 0.177 af

Link AP1: AP1

Subcatchment100: EX-WS-100

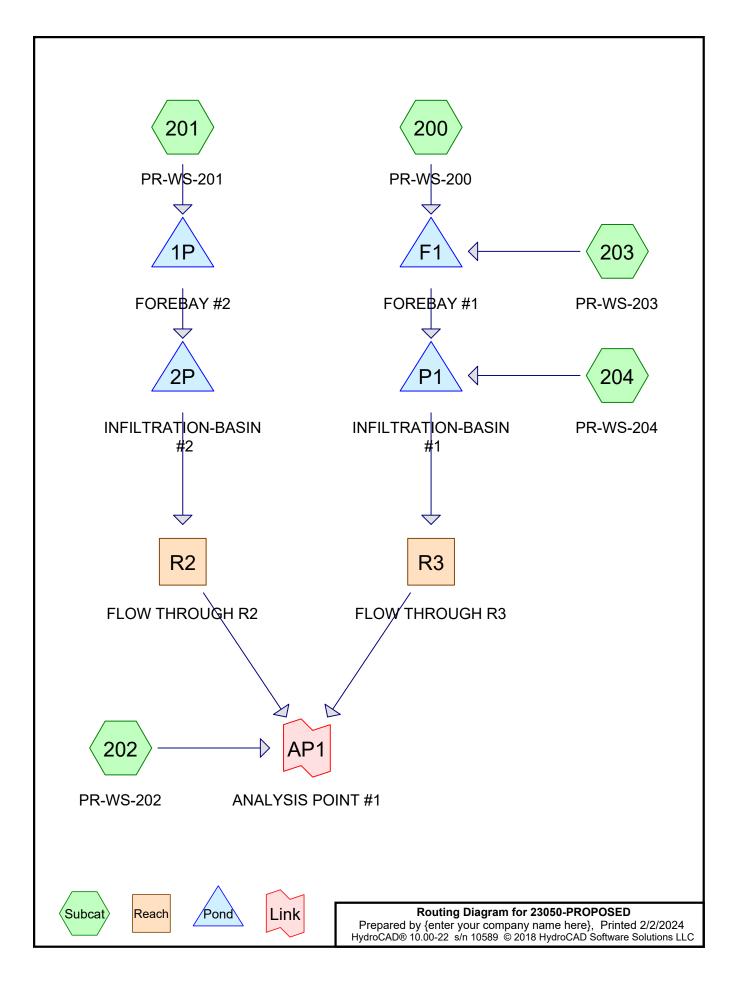
Inflow=1.35 cfs 0.177 af Primary=1.35 cfs 0.177 af

Total Runoff Area = 2.182 ac Runoff Volume = 0.177 af Average Runoff Depth = 0.98" 96.95% Pervious = 2.116 ac 3.05% Impervious = 0.067 ac

## APPENDIX II

## PROPOSED CONDITIONS DRAINAGE ANALYSIS

2 YEAR Summary Analysis 10 YEAR Complete Analysis 25 YEAR Summary Analysis 50 YEAR Summary Analysis



## 23050-PROPOSED

## Area Listing (all nodes)

| Area    | CN | CN Description                               |  |
|---------|----|--|--|
| (acres) |    | (subcatchment-numbers)                       |  |
| 1.307   | 39 | GRASS COVER >75%, HSG A (200, 201, 202, 203) |  |
| 0.330   | 98 | IMPERVIOUS AREA, HSG A (200)                 |  |
| 0.304   | 98 | IMPERVIOUS, HSG A (201)                      |  |
| 0.241   | 98 | Roofs, HSG A (204)                           |  |
| 2.182   | 63 | TOTAL AREA                                   |  |

## Soil Listing (all nodes)

| Area    | Soil  | Subcatchment            |
|---------|-------|-------------------------|
| (acres) | Group | Numbers                 |
| 2.182   | HSG A | 200, 201, 202, 203, 204 |
| 0.000   | HSG B |                         |
| 0.000   | HSG C |                         |
| 0.000   | HSG D |                         |
| 0.000   | Other |                         |
| 2.182   |       | TOTAL AREA              |
|         | Othor | TOTAL AREA              |

Type III 24-hr 2 YEAR Rainfall=3.08" Printed 2/2/2024

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Page 4

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

| Subcatchment200: PR-WS-200                   | Runoff Area=21,280 sf 67.50% Impervious Runoff Depth>1.25"<br>Tc=7.0 min CN=79 Runoff=0.67 cfs 0.051 af                             |
|--|---|
| Subcatchment201: PR-WS-201                   | Runoff Area=21,663 sf 61.18% Impervious Runoff Depth>1.01"<br>Tc=7.0 min CN=75 Runoff=0.54 cfs 0.042 af                             |
| Subcatchment202: PR-WS-202                   | Runoff Area=31,076 sf 0.00% Impervious Runoff Depth=0.00"<br>Tc=7.0 min CN=39 Runoff=0.00 cfs 0.000 af                              |
| Subcatchment203: PR-WS-203                   | Runoff Area=10,516 sf 0.00% Impervious Runoff Depth=0.00"<br>Tc=7.0 min CN=39 Runoff=0.00 cfs 0.000 af                              |
| Subcatchment204: PR-WS-204                   | Runoff Area=10,502 sf 100.00% Impervious Runoff Depth>2.85"<br>Tc=7.0 min CN=98 Runoff=0.69 cfs 0.057 af                            |
| Reach R2: FLOW THROUGH R2<br>n=0.022         | Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=124.0' S=0.1532 '/' Capacity=200.21 cfs Outflow=0.00 cfs 0.000 af |
| Reach R3: FLOW THROUGH R3<br>n=0.022         | Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=130.0' S=0.1846 '/' Capacity=368.09 cfs Outflow=0.00 cfs 0.000 af |
| Pond 1P: FOREBAY#2                           | Peak Elev=94.61' Storage=277 cf Inflow=0.54 cfs 0.042 af<br>Outflow=0.52 cfs 0.037 af   |
| Pond 2P: INFILTRATION-BASIN#2<br>Discarded=0 | Peak Elev=93.79' Storage=492 cf Inflow=0.52 cfs 0.037 af<br>0.08 cfs 0.036 af Primary=0.00 cfs 0.000 af Outflow=0.08 cfs 0.036 af   |
| Pond F1: FOREBAY#1                           | Peak Elev=91.07' Storage=670 cf Inflow=0.67 cfs 0.051 af<br>Outflow=0.43 cfs 0.036 af   |
| Pond P1: INFILTRATION-BASIN#1<br>Discarded=0 | Peak Elev=90.79' Storage=1,207 cf Inflow=0.82 cfs 0.094 af<br>0.16 cfs 0.093 af Primary=0.00 cfs 0.000 af Outflow=0.16 cfs 0.093 af |
| Link AP1: ANALYSISPOINT #1                   | Inflow=0.00 cfs 0.000 af<br>Primary=0.00 cfs 0.000 af   |

Total Runoff Area = 2.182 ac Runoff Volume = 0.150 af Average Runoff Depth = 0.82" 59.89% Pervious = 1.307 ac 40.11% Impervious = 0.875 ac

Type III 24-hr 10 YEAR Rainfall=4.63" Printed 2/2/2024

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

| Subcatchment200: PR-WS-200                      | Runoff Area=21,280 sf 67.50% Impervious Runoff Depth>2.48"<br>Tc=7.0 min CN=79 Runoff=1.36 cfs 0.101 af                           |
|---|---|
| Subcatchment201: PR-WS-201                      | Runoff Area=21,663 sf 61.18% Impervious Runoff Depth>2.15"<br>Tc=7.0 min CN=75 Runoff=1.19 cfs 0.089 af                           |
| Subcatchment202: PR-WS-202                      | Runoff Area=31,076 sf 0.00% Impervious Runoff Depth>0.13"<br>Tc=7.0 min CN=39 Runoff=0.01 cfs 0.008 af                            |
| Subcatchment203: PR-WS-203                      | Runoff Area=10,516 sf 0.00% Impervious Runoff Depth>0.13"<br>Tc=7.0 min CN=39 Runoff=0.00 cfs 0.003 af                            |
| Subcatchment204: PR-WS-204                      | Runoff Area=10,502 sf 100.00% Impervious Runoff Depth>4.39"<br>Tc=7.0 min CN=98 Runoff=1.04 cfs 0.088 af                          |
| Reach R2: FLOW THROUGH R2<br>n=0.022 L=         | Avg. Flow Depth=0.02' Max Vel=1.40 fps Inflow=0.03 cfs 0.001 af 124.0' S=0.1532 '/' Capacity=200.21 cfs Outflow=0.03 cfs 0.001 af |
| Reach R3: FLOW THROUGH R3<br>n=0.022 L=         | Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af 130.0' S=0.1846 '/' Capacity=368.09 cfs Outflow=0.00 cfs 0.000 af |
| Pond 1P: FOREBAY#2                              | Peak Elev=94.69' Storage=313 cf Inflow=1.19 cfs 0.089 af<br>Outflow=1.17 cfs 0.084 af   |
|   | Peak Elev=94.53' Storage=1,495 cf Inflow=1.17 cfs 0.084 af<br>4 cfs 0.082 af Primary=0.03 cfs 0.001 af Outflow=0.17 cfs 0.083 af  |
| Pond F1: FOREBAY#1                              | Peak Elev=91.50' Storage=1,060 cf Inflow=1.36 cfs 0.104 af<br>Outflow=1.32 cfs 0.089 af   |
| Pond P1: INFILTRATION-BASIN#1<br>Discarded=0.24 | Peak Elev=91.50' Storage=2,611 cf Inflow=2.34 cfs 0.178 af<br>4 cfs 0.177 af Primary=0.00 cfs 0.000 af Outflow=0.24 cfs 0.177 af  |
| Link AP1: ANALYSISPOINT #1                      | Inflow=0.04 cfs 0.009 af<br>Primary=0.04 cfs 0.009 af   |

Total Runoff Area = 2.182 ac Runoff Volume = 0.289 af Average Runoff Depth = 1.59" 59.89% Pervious = 1.307 ac 40.11% Impervious = 0.875 ac

Type III 24-hr 10 YEAR Rainfall=4.63" Printed 2/2/2024 ns LLC Page 2

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## Summary for Subcatchment 200: PR-WS-200

Runoff = 1.36 cfs @ 12.10 hrs, Volume= 0.101 af, Depth> 2.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.63"

|   | A                                       | rea (sf)         | CN               | Description            |                   |               |  |  |
|---|---|------------------|------------------|------------------------|-------------------|---------------|--|--|
| * |   | 14,365           | 98               | IMPERVIO               | US AREA,          | HSG A         |  |  |
| * |   | 6,915            | 39               | GRASS CC               | OVER >75%         | %, HSG A      |  |  |
|   |   | 21,280           | 79               | Weighted A             | verage            |               |  |  |
|   |   | 6,915            |                  | 32.50% Pe              | rvious Area       | 3             |  |  |
|   |   | 14,365           |                  | 67.50% Impervious Area |                   |               |  |  |
|   | Tc<br>(min)                             | Length<br>(feet) | Slope<br>(ft/ft) | ,                      | Capacity<br>(cfs) | Description   |  |  |
|   | 7.0                                     |                  |                  |                        |                   | Direct Entry, |  |  |
|   | Summary for Subcatchment 201: PR-WS-201 |                  |                  |                        |                   |               |  |  |

## Runoff = 1.19 cfs @ 12.11 hrs, Volume= 0.089 af, Depth> 2.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.63"

| _ | A           | rea (sf)                  | CN               | Description                            |                   |               |  |
|---|-------------|---------------------------|------------------|--|-------------------|---------------|--|
| * |             | 13,253                    | 98               | IMPERVIOUS, HSG A                      |                   |               |  |
| * |             | 8,410                     | 39               | GRASS CC                               | VER >75%          | %, HSG A      |  |
| _ |             | 21,663<br>8,410<br>13,253 |                  | Weighted A<br>38.82% Pei<br>61.18% Imp | vious Area        |               |  |
|   | Tc<br>(min) | Length<br>(feet)          | Slope<br>(ft/ft) |  | Capacity<br>(cfs) | I             |  |
|   | 7.0         |                           |                  |  |                   | Direct Entry, |  |
|   |             |                           |                  |  |                   |               |  |

## Summary for Subcatchment 202: PR-WS-202

Runoff = 0.01 cfs @ 14.55 hrs, Volume= 0.008 af, Depth> 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.63"

|   | Area (sf) | CN | Description             |
|---|-----------|----|-------------------------|
| * | 31,076    | 39 | GRASS COVER >75%, HSG A |
|   | 31,076    |    | 100.00% Pervious Area   |

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|---|--|--|--|--|--|--|
| HydroCAD® 10.00-22 s/n 10589 © 2018 HydroCAD Software Solutions LLC Page 3  |  |  |  |  |  |  |
| Tc Length Slope Velocity Capacity Description<br>(min) (feet) (ft/ft) (ft/sec) (cfs)  |  |  |  |  |  |  |
| 7.0 Direct Entry,   |  |  |  |  |  |  |
| Summary for Subcatchment 203: PR-WS-203   |  |  |  |  |  |  |
| Runoff = 0.00 cfs @ 14.55 hrs, Volume= 0.003 af, Depth> 0.13"   |  |  |  |  |  |  |
| Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs<br>Type III 24-hr  10 YEAR Rainfall=4.63"  |  |  |  |  |  |  |
| Area (sf) CN Description  |  |  |  |  |  |  |
| * 10,516 39 GRASS COVER >75%, HSG A   |  |  |  |  |  |  |
| 10,516 100.00% Pervious Area  |  |  |  |  |  |  |
| Tc Length Slope Velocity Capacity Description<br>(min) (feet) (ft/ft) (ft/sec) (cfs)  |  |  |  |  |  |  |
| 7.0 Direct Entry,   |  |  |  |  |  |  |
| Summary for Subcatchment 204: PR-WS-204   |  |  |  |  |  |  |
| Runoff = 1.04 cfs @ 12.10 hrs, Volume= 0.088 af, Depth> 4.39"   |  |  |  |  |  |  |
| Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs<br>Type III 24-hr  10 YEAR Rainfall=4.63"  |  |  |  |  |  |  |
| Area (sf) CN Description  |  |  |  |  |  |  |
| 10,502 98 Roofs, HSG A  |  |  |  |  |  |  |
| 10,502 100.00% Impervious Area  |  |  |  |  |  |  |
| Tc Length Slope Velocity Capacity Description<br>(min) (feet) (ft/ft) (ft/sec) (cfs)  |  |  |  |  |  |  |
| 7.0Direct Entry,  |  |  |  |  |  |  |
| Summary for Reach R2: FLOW THROUGH R2   |  |  |  |  |  |  |
| Inflow Area =       0.497 ac, 61.18% Impervious, Inflow Depth = 0.03" for 10 YEAR event         Inflow =       0.03 cfs @ 12.79 hrs, Volume=       0.001 af         Outflow =       0.03 cfs @ 12.81 hrs, Volume=       0.001 af, Atten= 0%, Lag= 1.2 min |  |  |  |  |  |  |
| Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs<br>Max. Velocity= 1.40 fps, Min. Travel Time= 1.5 min<br>Avg. Velocity = 1.20 fps, Avg. Travel Time= 1.7 min  |  |  |  |  |  |  |
| Peak Storage= 3 cf @ 12.81 hrs  |  |  |  |  |  |  |

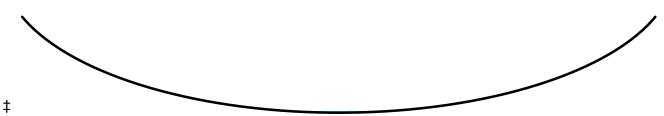
Type III 24-hr 10 YEAR Rainfall=4.63"

Peak Storage= 3 cf @ 12.81 hrs Average Depth at Peak Storage= 0.02' Bank-Full Depth= 1.00' Flow Area= 10.0 sf, Capacity= 200.21 cfs

23050-PROPOSED

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15.00' x 1.00' deep Parabolic Channel, n= 0.022 Earth, clean & straight Length= 124.0' Slope= 0.1532 '/' Inlet Invert= 87.00', Outlet Invert= 68.00'



## Summary for Reach R3: FLOW THROUGH R3

| Inflow Area | a = | 0.971 ac, 58 | 8.79% Impervious, I | nflow Depth = 0.00" | for 10 YEAR event    |
|-------------|-----|--------------|---------------------|---------------------|----------------------|
| Inflow      | =   | 0.00 cfs @   | 0.00 hrs, Volume=   | 0.000 af            |                      |
| Outflow     | =   | 0.00 cfs @   | 0.00 hrs, Volume=   | 0.000 af, Atte      | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs Average Depth at Peak Storage= 0.00' Bank-Full Depth= 1.00' Flow Area= 16.7 sf, Capacity= 368.09 cfs

25.00' x 1.00' deep Parabolic Channel, n= 0.022 Earth, clean & straight Length= 130.0' Slope= 0.1846 '/' Inlet Invert= 92.00', Outlet Invert= 68.00'



## Summary for Pond 1P: FOREBAY #2

| Inflow Area = | 0.497 ac, 61.18% Impervious, Inflow D | Depth > 2.15" for 10 YEAR event   |
|---------------|---------------------------------------|-----------------------------------|
| Inflow =      | 1.19 cfs @ 12.11 hrs, Volume=         | 0.089 af                          |
| Outflow =     | 1.17 cfs @_ 12.12 hrs, Volume=        | 0.084 af, Atten= 2%, Lag= 0.9 min |
| Primary =     | 1.17 cfs @_ 12.12 hrs, Volume=        | 0.084 af                          |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 94.69' @ 12.12 hrs Surf.Area= 467 sf Storage= 313 cf

Plug-Flow detention time= 44.6 min calculated for 0.084 af (94% of inflow) Center-of-Mass det. time= 13.0 min (851.9 - 838.8)

 Type III 24-hr
 10 YEAR Rainfall=4.63"

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| Volume   | Inve                      | ert Avail                               | .Storage                                  | Storage Descripti   | on  |  |  |
|--|---------------------------|---|---|---|---|--|--|
| #1   | 93.0                      | )0'                                     | 480 cf                                    | Custom Stage D  | ata (Irregular)Liste                        | ed below (Recalc)  |  |
| Elevation<br>(feet)<br>93.00<br>94.00<br>95.00 | )<br>)<br>)               | Surf.Area<br>(sq-ft)<br>5<br>214<br>613 | Perim.<br>(feet)<br>8.5<br>133.0<br>149.0 | Inc.Store<br>(cubic-feet)<br>0<br>84<br>396                 | Cum.Store<br>(cubic-feet)<br>0<br>84<br>480 | Wet.Area<br>(sq-ft)<br>5<br>1,409<br>1,794   |  |
|  | <u>Routing</u><br>Primary |   | .50' <b>6.0'</b><br>Head<br>2.50<br>Coet  | d (feet) 0.20 0.40<br>3.00 3.50 4.00<br>f. (English) 2.38 2 | 0.60 0.80 1.00 1<br>4.50 5.00 5.50          | <b>Rectangular Weir</b><br>1.20 1.40 1.60 1.80 2.0<br>37 2.67 2.65 2.66 2.66<br>32 |  |

Primary OutFlow Max=1.13 cfs @ 12.12 hrs HW=94.68' TW=93.95' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 1.13 cfs @ 1.02 fps)

## Summary for Pond 2P: INFILTRATION-BASIN #2

[58] Hint: Peaked 0.53' above defined flood level

| Inflow Area = | 0.497 ac, 61.18% Impervious, Inflow D | epth > 2.02" for 10 YEAR event      |
|---------------|---------------------------------------|-------------------------------------|
| Inflow =      | 1.17 cfs @ 12.12 hrs, Volume=         | 0.084 af                            |
| Outflow =     | 0.17 cfs @ 12.79 hrs, Volume=         | 0.083 af, Atten= 86%, Lag= 39.8 min |
| Discarded =   | 0.14 cfs @ 12.79 hrs, Volume=         | 0.082 af                            |
| Primary =     | 0.03 cfs @ 12.79 hrs, Volume=         | 0.001 af                            |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 94.53' @ 12.79 hrs Surf.Area= 1,695 sf Storage= 1,495 cf Flood Elev= 94.00' Surf.Area= 1,237 sf Storage= 726 cf

Plug-Flow detention time= 131.4 min calculated for 0.083 af (99% of inflow) Center-of-Mass det. time= 127.4 min ( 979.2 - 851.9 )

| Volume                                   | Inver   | rt Avail.                                     | Storage                                     | Storage Descripti                              | on  |  |  |
|--|---|---|---|--|---|--|--|
| #1                                       | 93.00   | )' :  | 2,407 cf                                    | Custom Stage D                                 | ata (Irregular)Lisi                                   | ed below (Recalc)  |  |
| Elevatio<br>(fee<br>93.0<br>94.0<br>95.0 | 20<br>20<br>20  | Surf.Area<br>(sq-ft)<br>316<br>1,237<br>2,168 | Perim.<br>(feet)<br>209.0<br>311.0<br>326.0 | Inc.Store<br>(cubic-feet)<br>0<br>726<br>1,681 | Cum.Store<br>(cubic-feet)<br>0<br>726<br>2,407        | Wet.Area<br>(sq-ft)<br>316<br>4,545<br>5,369   |  |
| Device<br>#1                             | Routing   | Inv   | ••••  | et Devices                                     | od Voo/Trap Wai                                       | $c_{1} = 251(C - 314)$   |  |
| #1<br>#2<br>#3                           | #2 Device 3 94.50' <b>4.0'</b><br>#3 Primary 94.50' <b>10.</b><br>Hea |   | 50' <b>4.0'</b><br>50' <b>10.0</b><br>Head  | long Sharp-Crest<br>' long x 6.0' brea         | ed Rectangular V<br>dth Emergency S<br>0.60 0.80 1.00 | r Cv= 2.51 (C= 3.14)<br>Veir 2 End Contraction(s<br>Spillway<br>1.20 1.40 1.60 1.80 2. |  |

Type III 24-hr 10 YEAR Rainfall=4.63" Printed 2/2/2024 ns LLC Page 6

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|    |           |        | Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67  | 2.65 2.65 2.65  |
|----|-----------|--------|--|-----------------|
|    |           |        | 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83        |                 |
| #4 | Discarded | 93.00' | 3.000 in/hr Exfiltration over Surface area     |                 |
|    |           |        | Conductivity to Groundwater Elevation = 88.00' | Phase-In= 0.10' |

**Discarded OutFlow** Max=0.14 cfs @ 12.79 hrs HW=94.53' (Free Discharge) **4=Exfiltration** (Controls 0.14 cfs)

Primary OutFlow Max=0.03 cfs @ 12.79 hrs HW=94.53' TW=87.02' (Dynamic Tailwater) 3=Emergency Spillway (Passes 0.03 cfs of 0.10 cfs potential flow) 2=Sharp-Crested Rectangular Weir (Passes 0.03 cfs of 0.06 cfs potential flow)

**1=Sharp-Crested Vee/Trap Weir** (Weir Controls 0.03 cfs @ 0.72 fps)

## Summary for Pond F1: FOREBAY #1

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=44)

| Inflow Area = | 0.730 ac, 45.18% Impervious, Inflow D | Depth > 1.71" for 10 YEAR event   |
|---------------|---------------------------------------|-----------------------------------|
| Inflow =      | 1.36 cfs @ 12.10 hrs, Volume=         | 0.104 af                          |
| Outflow =     | 1.32 cfs @ 12.12 hrs, Volume=         | 0.089 af, Atten= 3%, Lag= 1.1 min |
| Primary =     | 1.32 cfs @ 12.12 hrs, Volume=         | 0.089 af                          |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 91.50' @ 13.05 hrs Surf.Area= 993 sf Storage= 1,060 cf

Plug-Flow detention time= 109.4 min calculated for 0.089 af (86% of inflow) Center-of-Mass det. time= 47.9 min ( 881.4 - 833.5 )

| Volume           | Inve    | ert Avail            | .Storage         | Storage Descripti                     | on                          |                             |    |
|------------------|---------|----------------------|------------------|---------------------------------------|-----------------------------|-----------------------------|----|
| #1               | 90.0    | )0'                  | 1,612 cf         | Custom Stage D                        | <b>ata (Irregular)</b> List | ed below (Recalc)           |    |
| Elevatio<br>(fee |         | Surf.Area<br>(sq-ft) | Perim.<br>(feet) | Inc.Store<br>(cubic-feet)             | Cum.Store<br>(cubic-feet)   | Wet.Area<br>(sq-ft <u>)</u> |    |
| 90.0             | 0       | 455                  | 91.0             | 0                                     | 0                           | 455                         |    |
| 92.0             | 0       | 1,218                | 167.0            | 1,612                                 | 1,612                       | 2,037                       |    |
| Device           | Routing | Inv                  | vert Outle       | et Devices                            |                             |                             |    |
| #1               | Primary | 91                   | .00' 10.0        | long x 7.0' brea                      | dth Broad-Creste            | ed Rectangular Weir         |    |
|                  | -       |                      | Hea              | d (feet) 0.20 0.40                    | 0.60 0.80 1.00              | 1.20 1.40 1.60 1.80 2.      | 00 |
|                  |         |                      | 2.50             | 3.00 3.50 4.00                        | 4.50 5.00 5.50              |                             |    |
|                  |         |                      |                  | f. (English) 2.40 2<br>2.66 2.65 2.66 |                             | 68 2.67 2.66 2.65 2.65      | 5  |
|                  |         |                      | 2.00             | 2.00 2.00 2.00 /                      | 2.00 2.10 2.13 2            | .10                         |    |

Primary OutFlow Max=1.28 cfs @ 12.12 hrs HW=91.14' TW=90.91' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir**(Weir Controls 1.28 cfs @ 0.90 fps)

## Summary for Pond P1: INFILTRATION-BASIN #1

[80] Warning: Exceeded Pond F1 by 0.09' @ 12.25 hrs (2.43 cfs 0.139 af)

| Inflow Area = | 0.971 ac, 58.79% Impervious, Inflow D     | Depth > 2.19" for 10 YEAR event     |
|---------------|---|-------------------------------------|
| Inflow =      | 2.34 cfs @ 12.11 hrs, Volume=             | 0.178 af                            |
| Outflow =     | 0.24 cfs @13.00 hrs, Volume=              | 0.177 af, Atten= 90%, Lag= 53.2 min |
| Discarded =   | 0.24 cfs @13.00 hrs, Volume=              | 0.177 af                            |
| Primary =     | 0.00 cfs $\overline{@}$ 0.00 hrs, Volume= | 0.000 af                            |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 91.50' @ 13.00 hrs Surf.Area= 2,214 sf Storage= 2,611 cf Flood Elev= 94.00' Surf.Area= 5,895 sf Storage= 12,044 cf

Plug-Flow detention time= 121.3 min calculated for 0.177 af (99% of inflow) Center-of-Mass det. time= 118.0 min (934.0 - 816.0)

| Volume               | Invert    | Avail.Sto             | orage                             | Storage Description   | n   |   |
|----------------------|-----------|-----------------------|-----------------------------------|---|---|---|
| #1                   | 90.00'    | 90.00' 12,044 cf      |                                   | Custom Stage Data (Irregular)Listed below (Recalc)                        |   | below (Recalc)                                |
| Elevatio<br>(fee     |           | ırf.Area F<br>(sq-ft) | Perim.<br>(feet)                  | Inc.Store<br>(cubic-feet)   | Cum.Store<br>(cubic-feet)                               | Wet.Area<br>(sq-ft)                           |
| 90.0<br>92.0<br>94.0 | 00        | ,                     | 189.0<br>229.0<br>397.0           | 0<br>3,805<br>8,238   | 0<br>3,805<br>12,044                                    | 1,306<br>2,701<br>11,093                      |
| Device               | Routing   | Invert                | Outl                              | et Devices  |   |   |
| #1                   | Device 2  | 93.50'                |                                   | ' long Sharp-Crest<br>Crest Height  | ed Rectangular Wo                                       | eir 2 End Contraction(s)                      |
| #2                   | Device 3  | 91.25'                | 45.0                              | deg x 1.75' rise Sh<br>2.56 (C= 3.20)                                     | arp-Crested Vee/  | Frap Weir                                     |
| #3                   | Primary   | 93.50'                | <b>10.0</b><br>Hea<br>2.50<br>Coe | <b>' long x 6.0' bread</b><br>d (feet) 0.20 0.40 (<br>0 3.00 3.50 4.00 4. | 0.60 0.80 1.00 1.2<br>50 5.00 5.50<br>51 2.70 2.68 2.68 | 20 1.40 1.60 1.80 2.00<br>2.67 2.65 2.65 2.65 |
| #4                   | Discarded | 90.00'                | Con                               | 0 in/hr Exfiltration<br>ductivity to Groundw                              | ater Elevation = 88                                     | .00' Phase-In= 0.10'                          |

**Discarded OutFlow** Max=0.24 cfs @ 13.00 hrs HW=91.50' (Free Discharge) **4=Exfiltration** (Controls 0.24 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=90.00' TW=92.00' (Dynamic Tailwater) -3=EMERGENCY SPILLWAY (Controls 0.00 cfs)

-2=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs) —1=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

## Summary for Link AP1: ANALYSIS POINT #1

| Inflow Area | = | 2.182 ac, 4 | 0.11% Imp  | ervious, | Inflow De | pth > 0  | .05"   | for 10  | YEAR event  |   |
|-------------|---|-------------|------------|----------|-----------|----------|--------|---------|-------------|---|
| Inflow =    | = | 0.04 cfs @  | 12.85 hrs, | Volume   | =         | 0.009 af |        |         |             |   |
| Primary =   | = | 0.04 cfs @  | 12.85 hrs, | Volume   | =         | 0.009 af | , Atte | en= 0%, | Lag= 0.0 mi | n |

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Type III 24-hr 25 YEAR Rainfall=5.84" Printed 2/2/2024

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

| Subcatchment200: PR-WS-200                     | Runoff Area=21,280 sf 67.50% Impervious Runoff Depth>3.53"<br>Tc=7.0 min CN=79 Runoff=1.93 cfs 0.144 af                               |
|--|---|
| Subcatchment201: PR-WS-201                     | Runoff Area=21,663 sf 61.18% Impervious Runoff Depth>3.14"<br>Tc=7.0 min CN=75 Runoff=1.75 cfs 0.130 af                               |
| Subcatchment202: PR-WS-202                     | Runoff Area=31,076 sf 0.00% Impervious Runoff Depth>0.40"<br>Tc=7.0 min CN=39 Runoff=0.11 cfs 0.024 af                                |
| Subcatchment203: PR-WS-203                     | Runoff Area=10,516 sf 0.00% Impervious Runoff Depth>0.40"<br>Tc=7.0 min CN=39 Runoff=0.04 cfs 0.008 af                                |
| Subcatchment204: PR-WS-204                     | Runoff Area=10,502 sf 100.00% Impervious Runoff Depth>5.60"<br>Tc=7.0 min CN=98 Runoff=1.32 cfs 0.112 af                              |
| Reach R2: FLOW THROUGH R2<br>n=0.022 L=        | Avg. Flow Depth=0.05' Max Vel=2.78 fps Inflow=0.32 cfs 0.024 af =124.0' S=0.1532 '/' Capacity=200.21 cfs Outflow=0.32 cfs 0.024 af    |
| Reach R3: FLOW THROUGH R3<br>n=0.022 L=        | Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af<br>=130.0' S=0.1846 '/' Capacity=368.09 cfs Outflow=0.00 cfs 0.000 af |
| Pond 1P: FOREBAY#2                             | Peak Elev=94.78' Storage=359 cf Inflow=1.75 cfs 0.130 af<br>Outflow=1.73 cfs 0.125 af   |
| Pond 2P: INFILTRATION-BASIN#2<br>Discarded=0.1 | Peak Elev=94.78' Storage=1,956 cf Inflow=1.73 cfs 0.125 af<br>6 cfs 0.098 af Primary=0.32 cfs 0.024 af Outflow=0.48 cfs 0.123 af      |
| Pond F1: FOREBAY#1                             | Peak Elev=91.98' Storage=1,583 cf Inflow=1.93 cfs 0.152 af<br>Outflow=1.85 cfs 0.137 af   |
| Pond P1: INFILTRATION-BASIN#1<br>Discarded=0.3 | Peak Elev=91.98' Storage=3,746 cf Inflow=3.16 cfs 0.249 af<br>0 cfs 0.244 af Primary=0.00 cfs 0.000 af Outflow=0.30 cfs 0.244 af      |
| Link AP1: ANALYSISPOINT #1                     | Inflow=0.42 cfs 0.048 af<br>Primary=0.42 cfs 0.048 af   |

Total Runoff Area = 2.182 ac Runoff Volume = 0.418 af Average Runoff Depth = 2.30" 59.89% Pervious = 1.307 ac 40.11% Impervious = 0.875 ac

Type III 24-hr 50 YEAR Rainfall=6.96" Printed 2/2/2024

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

| Subcatchment200: PR-WS-200                    | Runoff Area=21,280 sf 67.50% Impervious Runoff Depth>4.54"<br>Tc=7.0 min CN=79 Runoff=2.47 cfs 0.185 af                               |
|---|---|
| Subcatchment201: PR-WS-201                    | Runoff Area=21,663 sf 61.18% Impervious Runoff Depth>4.11"<br>Tc=7.0 min CN=75 Runoff=2.29 cfs 0.170 af                               |
| Subcatchment202: PR-WS-202                    | Runoff Area=31,076 sf 0.00% Impervious Runoff Depth>0.75"<br>Tc=7.0 min CN=39 Runoff=0.28 cfs 0.045 af                                |
| Subcatchment203: PR-WS-203                    | Runoff Area=10,516 sf 0.00% Impervious Runoff Depth>0.75"<br>Tc=7.0 min CN=39 Runoff=0.09 cfs 0.015 af                                |
| Subcatchment204: PR-WS-204                    | Runoff Area=10,502 sf  100.00% Impervious  Runoff Depth>6.72"<br>Tc=7.0 min  CN=98  Runoff=1.57 cfs  0.135 af                         |
| Reach R2: FLOW THROUGH R2<br>n=0.022 L        | Avg. Flow Depth=0.07' Max Vel=3.51 fps Inflow=0.68 cfs 0.050 af .=124.0' S=0.1532 '/' Capacity=200.21 cfs Outflow=0.68 cfs 0.050 af   |
| Reach R3: FLOW THROUGH R3<br>n=0.022 L        | Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af<br>=130.0' S=0.1846 '/' Capacity=368.09 cfs Outflow=0.00 cfs 0.000 af |
| Pond 1P: FOREBAY#2                            | Peak Elev=94.95' Storage=448 cf Inflow=2.29 cfs 0.170 af<br>Outflow=2.25 cfs 0.165 af   |
| Pond 2P: INFILTRATION-BASIN#2<br>Discarded=0. | Peak Elev=94.94' Storage=2,284 cf Inflow=2.25 cfs 0.165 af<br>18 cfs 0.110 af Primary=0.68 cfs 0.050 af Outflow=0.86 cfs 0.161 af     |
| Pond F1: FOREBAY#1                            | Peak Elev=92.51' Storage=1,612 cf Inflow=2.54 cfs 0.200 af<br>Outflow=1.51 cfs 0.185 af   |
| Pond P1: INFILTRATION-BASIN#1<br>Discarded=0. | Peak Elev=92.51' Storage=5,282 cf Inflow=3.05 cfs 0.319 af<br>39 cfs 0.301 af Primary=0.00 cfs 0.000 af Outflow=0.39 cfs 0.301 af     |
| Link AP1: ANALYSISPOINT #1                    | Inflow=0.94 cfs 0.095 af<br>Primary=0.94 cfs 0.095 af   |

Total Runoff Area = 2.182 ac Runoff Volume = 0.550 af Average Runoff Depth = 3.03" 59.89% Pervious = 1.307 ac 40.11% Impervious = 0.875 ac

# APPENDIX III

Web Soil Survey



|            | MAP L   | EGEND            | )                            | MAP INFORMATION  |
|------------|---|------------------|------------------------------|--|
| Area of In | <b>terest (AOI)</b><br>Area of Interest (AOI) | 8                | Spoil Area<br>Stony Spot     | The soil surveys that comprise your AOI were mapped at 1:20,000.   |
| Soils      | Soil Map Unit Polygons                        | 03               | Very Stony Spot              | Warning: Soil Map may not be valid at this scale.  |
| ~          | Soil Map Unit Lines<br>Soil Map Unit Points   | \$<br>⊘          | Wet Spot<br>Other            | Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil   |
| —          | Point Features<br>Blowout                     | •••<br>Water Fea | Special Line Features        | line placement. The maps do not show the small areas of<br>contrasting soils that could have been shown at a more detailed<br>scale.   |
| ×          | Borrow Pit                                    | ~~<br>Transport  | Streams and Canals           | Please rely on the bar scale on each map sheet for map   |
| ¥<br>♦     | Clay Spot<br>Closed Depression                |                  | Rails<br>Interstate Highways | measurements. Source of Map: Natural Resources Conservation Service  |
| *          | Gravel Pit<br>Gravelly Spot                   | US Routes        | US Routes<br>Major Roads     | Web Soil Survey URL:<br>Coordinate System: Web Mercator (EPSG:3857)  |
| 0<br>1     | Landfill<br>Lava Flow                         | ~                |                              | Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts   |
| عليه       | Marsh or swamp                                | Backgrou         |                              | distance and area. A projection that preserves area, such as the<br>Albers equal-area conic projection, should be used if more<br>accurate calculations of distance or area are required.  |
| ☆<br>©     | Mine or Quarry<br>Miscellaneous Water         |                  |                              | This product is generated from the USDA-NRCS certified data as   |
| 0<br>~     | Perennial Water<br>Rock Outcrop               |                  |                              | of the version date(s) listed below.<br>Soil Survey Area: Strafford County, New Hampshire  |
| +          | Saline Spot<br>Sandy Spot                     |                  |                              | Survey Area Data: Version 24, Aug 22, 2023   |
| =          | Severely Eroded Spot                          |                  |                              | Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.  |
| ♦          | Sinkhole<br>Slide or Slip                     |                  |                              | Date(s) aerial images were photographed: Jun 19, 2020—Sep 20, 2020   |
| ø          | Sodic Spot                                    |                  |                              | The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. |

# **Map Unit Legend**

| Map Unit Symbol             | Map Unit Name                             | Acres in AOI | Percent of AOI |
|-----------------------------|---|--------------|----------------|
| BzB                         | Buxton silt loam, 3 to 8 percent slopes   | 0.2          | 4.8%           |
| Gv                          | Gravel and borrow pits                    | 2.1          | 43.2%          |
| W                           | Water                                     | 1.0          | 19.8%          |
| WdA                         | Windsor loamy sand, 0 to 3 percent slopes | 1.6          | 32.3%          |
| Totals for Area of Interest |   | 4.9          | 100.0%         |

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## **Strafford County, New Hampshire**

## BzB—Buxton silt loam, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d6p Elevation: 0 to 260 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Buxton and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Buxton**

#### Setting

Parent material: Glaciomarine

#### **Typical profile**

H1 - 0 to 10 inches: silt loam H2 - 10 to 28 inches: silty clay loam H3 - 28 to 43 inches: silty clay

#### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 12 to 24 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 7.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: C/D Ecological site: F145XY006CT - Semi-Rich Moist Lake Plain Hydric soil rating: No

#### **Minor Components**

#### Elmwood

*Percent of map unit:* 10 percent *Hydric soil rating:* No

#### Not named

*Percent of map unit:* 5 percent *Hydric soil rating:* No

## Gv—Gravel and borrow pits

#### Map Unit Setting

National map unit symbol: 9d7c Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Gravel and borrow pits:* 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Gravel And Borrow Pits**

#### **Typical profile**

*H1 - 0 to 6 inches:* extremely gravelly sand *H2 - 6 to 60 inches:* extremely gravelly sand

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

### W-Water

#### Map Unit Composition

*Water (less than 40 acres):* 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

### WdA—Windsor loamy sand, 0 to 3 percent slopes

#### Map Unit Setting

National map unit symbol: 2svkg Elevation: 0 to 990 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Farmland of local importance

#### Map Unit Composition

*Windsor, loamy sand, and similar soils:* 85 percent *Minor components:* 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Windsor, Loamy Sand**

#### Setting

Landform: Dunes, deltas, outwash terraces, outwash plains Landform position (three-dimensional): Tread, riser Down-slope shape: Convex, linear Across-slope shape: Convex, linear Parent material: Loose sandy glaciofluvial deposits derived from granite and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy glaciofluvial deposits derived from gneiss

#### **Typical profile**

O - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loamy sand

Bw - 3 to 25 inches: loamy sand

C - 25 to 65 inches: sand

#### **Properties and qualities**

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 3.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: A Ecological site: F144AY022MA - Dry Outwash Hydric soil rating: No

#### **Minor Components**

#### Deerfield, loamy sand

Percent of map unit: 10 percent Landform: Outwash plains, terraces, deltas Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Hinckley, loamy sand

Percent of map unit: 5 percent Landform: Outwash plains, eskers, kames, deltas Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Head slope, nose slope, side slope, crest, rise Down-slope shape: Convex

## Custom Soil Resource Report

Across-slope shape: Linear, convex Hydric soil rating: No

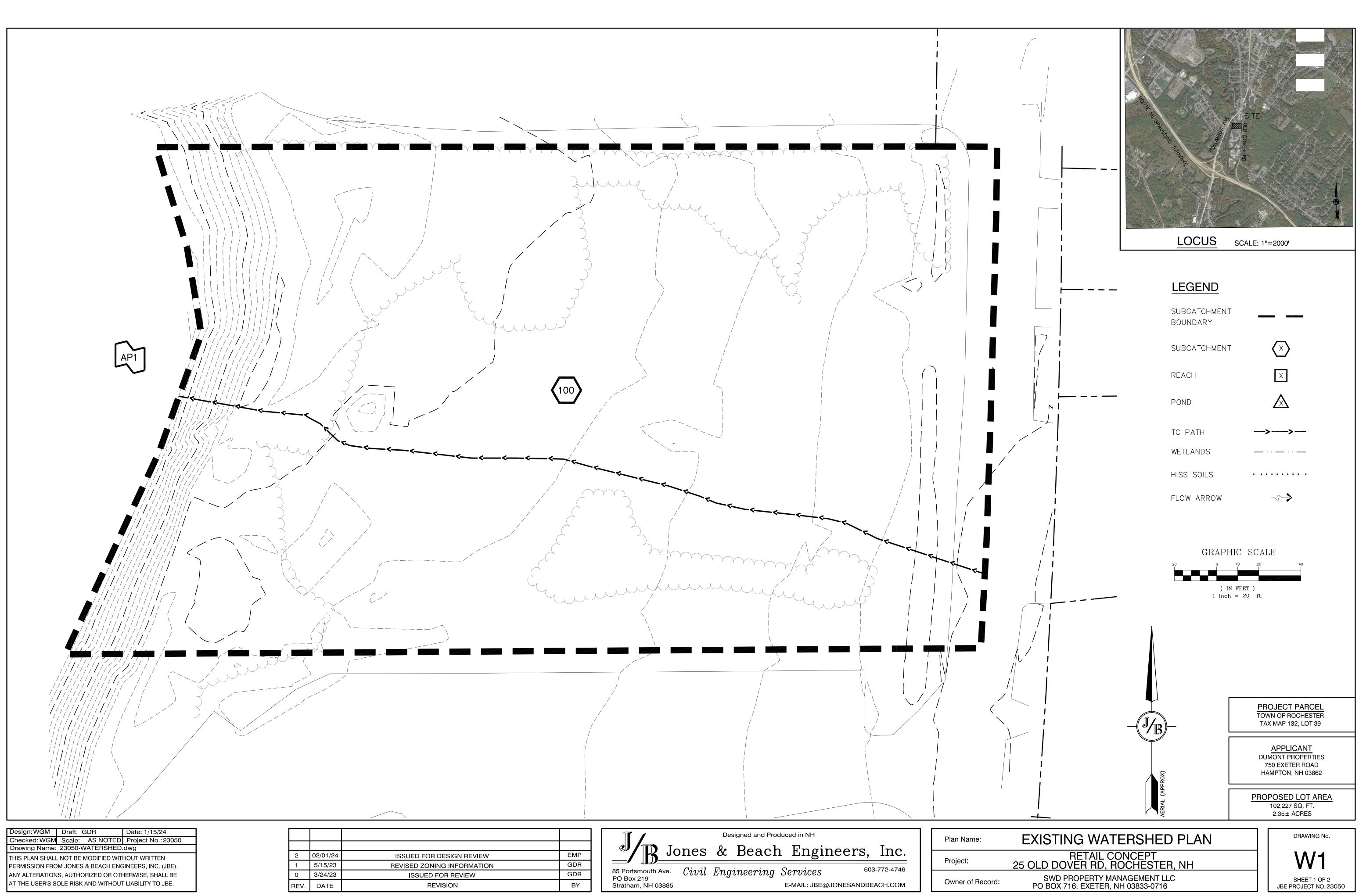
# APPENDIX IV

# Aerial Photograph of Site

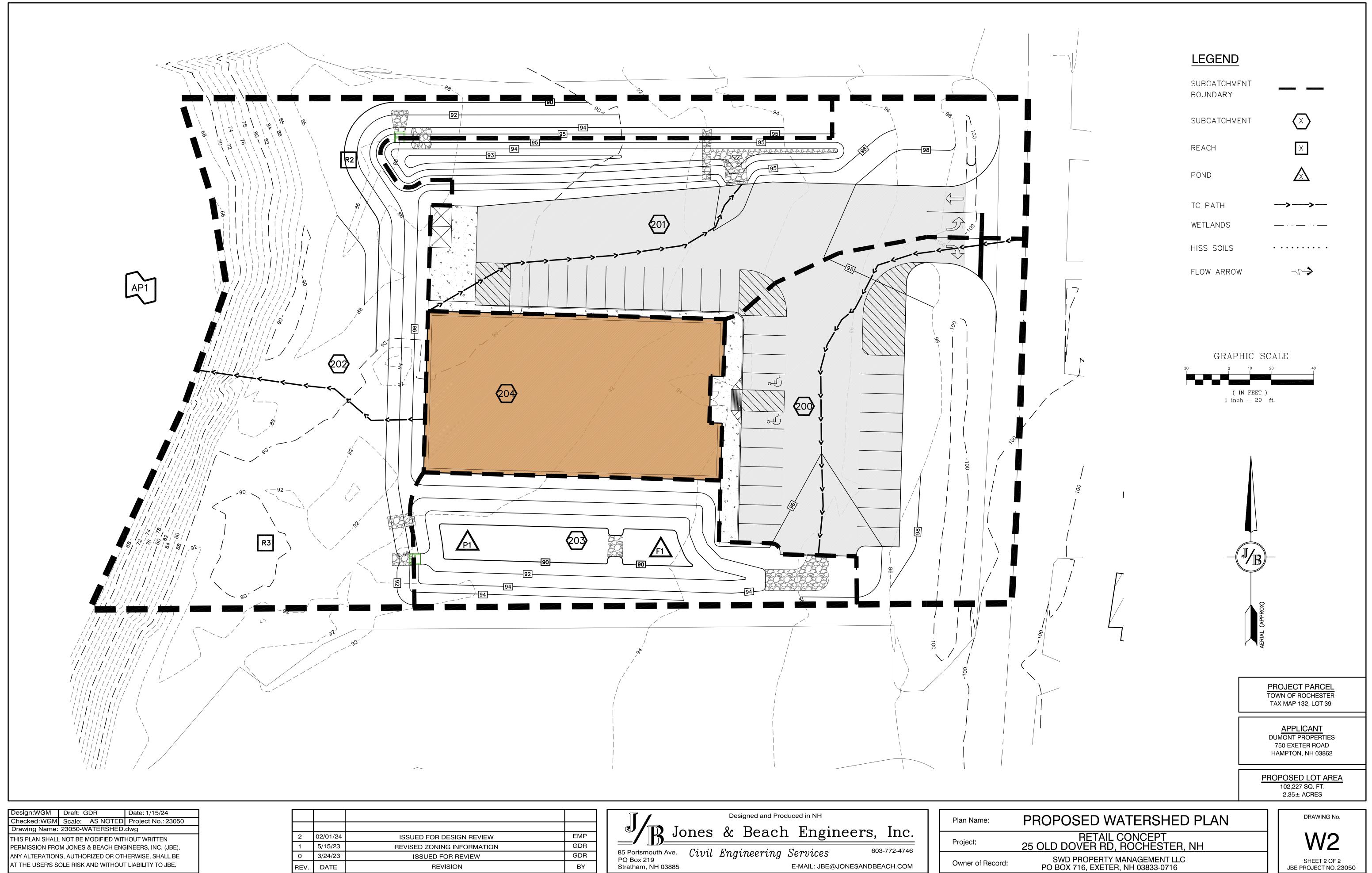


# APPENDIX V

Drainage Plans: Pre-Development Drainage Plan Post-Development Drainage Plan



| 2    | 02/01/24 | ISSUED FOR DESIGN REVIEW   |
|------|----------|----------------------------|
| 1    | 5/15/23  | REVISED ZONING INFORMATION |
| 0    | 3/24/23  | ISSUED FOR REVIEW          |
| REV. | DATE     | REVISION                   |



| Designed and Produce                        | ced in NH Plan Name:                           |
|---|--|
| Designed and Produce                        |  |
| EMP Jones & Beach                           | Eligineers, mc.                                |
| N GDR GDR                                   | Project:                                       |
| GDR 85 Portsmouth Ave. Civil Engineering Se |  |
|   | E-MAIL: JBE@JONESANDBEACH.COM Owner of Record: |